

# GATE 2020

Civil Engineering

Shift-1

Questions & Solutions



## SECTION: GENERAL APTITUDE

1. It is a common criticism that most of the academicians live in their\_\_\_\_\_. So, they are not aware of the real-life challenges.

- A. Ivory towers                      B. Homes  
C. Glass palaces                      D. Big flats

**Ans.** A

**Sol.** It is a common criticism that most of the academicians live in their **ivory tower**, so they are not aware of the real-life challenges.

2. His hunger for reading is insatiable. He reads indiscriminately. He is most certainly a/an \_\_\_\_\_ reader.

- A. all-round                              B. voracious  
C. wise                                      D. precocious

**Ans.** B

**Sol.** His hunger for reading is insatiable, he reads indiscriminately. He is most certainly a/an **voracious** reader.

3. Select the word that fits the analogy Fuse : Fusion ::  
Use : .....

- A. User                                      B. Uses  
C. Usage                                    D. Usion

**Ans.** C

**Sol.** Fuse : Fusion :: use : **Usage**

4. If 0, 1, 2, ..... 7, 8, 9 are coded as O, P, Q, ....., V, W, X, then 45 will be coded as

- A. TS                                        B. SS  
C. ST                                        D. SU

**Ans.** C

**Sol.**

0	1	2	3	4	5	6	7	8	9
O	P	Q	R	S	T	U	V	W	X

So, 45 → ST

5. The sum of two positive numbers is 100. After subtracting 5 from each number, the product of the resulting numbers is 0. One of the original numbers is

- A. 95                                        B. 85  
C. 80                                        D. 90

**Ans.** A

**Sol.** Let one positive number be a other positive number = 100 - a product of number after subtracting 5 from each number

$$\begin{aligned}
 &= (a - 5) \times (95 - a) = 0 \\
 \Rightarrow &95a - a^2 - 475 + 5a = 0 \\
 \Rightarrow &a^2 - 100a + 475 = 0 \\
 \Rightarrow &a^2 - 95a - 5a + 475 = 0 \\
 \Rightarrow &a(a - 95) - 5(a - 95) = 0 \\
 \Rightarrow &\text{either } a = 5 \text{ or } a = 95
 \end{aligned}$$

From, the options given 95 is the answer.

6. The American psychologist Howard Gardner expounds that human intelligence can be sub categorised into multiple kinds, in such a way that individuals differ with respect to their relative competence in each kind. Based on this theory, modern educationists insist on prescribing multi-dimensional curriculum and evaluation parameters that enable development and assessment of multiple intelligences.

Which of the following statements can be inferred from the given text?

- A. Howard Gardner insists that the teaching curriculum and evaluation needs to be multi-dimensional.  
B. Modern educationists want to develop and assess the theory of multiple intelligences.  
C. Modern educationists insist that the teaching curriculum and evaluation needs to be multi-dimensional.  
D. Howard Gardner wants to develop and assess the theory of multiple intelligences.

**Ans.** C

7. Five friends P, Q, R, S and T went camping. At night, they had to sleep in a row inside the tent. P, Q and T refused to sleep next to R since he snored loudly. P and S wanted to avoid Q as he usually hugged people in sleep.

Assuming everyone was satisfied with the sleeping arrangements, what is the order in which they slept?

- A. RSPTQ                      B. SPRTQ  
C. QTSPR                      D. QRSPT

**Ans.** A

**Sol.** Option A is the only arrangement where given conditions are met.

In option B & C, R is sleeping next to P

In option D, R is sleeping next to Q.

8. Insert seven numbers between 2 and 34, such that the resulting sequence including 2 and 34 is an arithmetic progression. The sum of these inserted seven numbers is .

- A. 124                          B. 130  
C. 120                          D. 126

**Ans.** D

**Sol.** As per the given question, the sequence of given AP is, 2 \_\_\_\_\_ 34

In this sequence first term (a) = 2

Last term (tn) = 34

So, as per the relation,

$$t_n = a + (n - 1) d$$

n → number of terms

d → common difference

$$34 = 2 + (9 - 1) d$$

$$d = 4$$

So, the A.P. becomes,

$$2, 6, 10, 14, 18, 22, 26, 30, 34$$

Sum of 7 terms between 2234 is 126

9. The unit's place in  $26591749^{110016}$  is

- A. 6                              B. 1  
C. 3                              D. 9

**Ans.** B

**Sol.** The unit digit in the power of 9 can be found by,

$$9^1 = 9 \rightarrow \text{unit digit is } 9$$

$$9^2 = 81 \rightarrow \text{so, unit digit is } 1$$

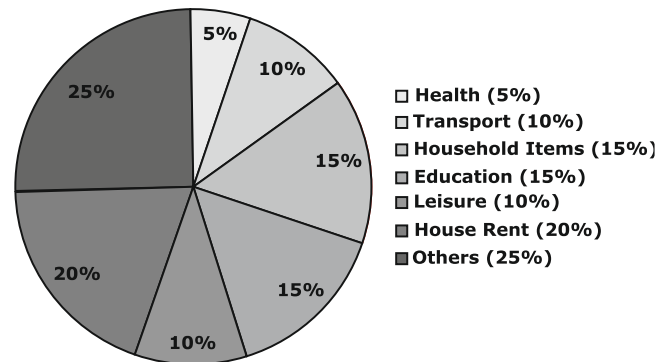
$$9^3 = 729 \rightarrow \text{unit digit is } 9$$

$$9^4 = 6561 \rightarrow \text{unit digit is } 1$$

So, from the above sequence, it follows that 9 power, if even the unit digit will be 1. and if 9 power, is odd unit digit will be 9 As per the question,  $26591749^{110016}$

The answer of unit digit will be 1.

10. The total expenditure of a family, on different activities in a month, is shown in the pie-chart. The extra money spent on education as compared to transport (in percent) is



- A. 50                              B. 100  
C. 33.3                          D. 55

**Ans.** A

**Sol.** Extra money spent on education as compared to transport

$$= \left( \frac{15 - 10}{10} \right) \times 100$$

$$= 50\%$$



$$\therefore V_c = \sqrt{gy_c}$$

$$\text{Now, } y_c = \left( \frac{q^2}{g} \right)^{1/3} = \left( \frac{\left( \frac{6}{4} \right)^2}{9.81} \right) = 0.612 \text{ m}$$

$$\left\{ \therefore q = \frac{Q}{B} \right\}$$

$$\therefore V_c = \sqrt{9.81 \times 0.612} = 2.44 \text{ m/sec.}$$

5. A fully submerged infinite sandy slope has an inclination of  $30^\circ$  with the horizontal. The saturated unit weight and effective angle of internal friction of sand are  $18 \text{ kN/m}^3$  and  $38^\circ$ , respectively. The unit weight of water is  $10 \text{ kN/m}^3$ . Assume that the seepage is parallel to the slope. Against shear failure of the slope, the factor of safety (round off to two decimal places) is

**Ans.** 0.6014

**Sol.** 
$$\text{FOS} = \frac{\gamma_{\text{sub}} \tan \phi}{\gamma_{\text{sat}} \tan \beta}$$

$$\text{FOS} = \frac{(18 - 10)}{18} \times \frac{\tan 38^\circ}{\tan 30^\circ} = 0.6014$$

6. An amount of 35.67 mg HCl is added to distilled water and the total solution volume is made to one litre. The atomic weights of H and Cl are 1 and 35.5, respectively. Neglecting the dissociation of water, the pH of the solution, is
- A. 3.50                      B. 2.50  
C. 2.01                      D. 3.01

**Ans.** D

**Sol.** 1 mole of HCl gives 1 mole  $\text{H}^+$  ions  
36.5 gm of HCl gives 1 gm of  $\text{H}^+$  ions  
Therefore,

35.67 mg of HCl gives,

$$\frac{1}{36.5} \times 36.67 \text{ mg of } \text{H}^+ \text{ ions}$$

$$\therefore 35.67 \text{ mg of HCl} = 0.977 \text{ mg of } \text{H}^+$$

Or 
$$\frac{0.977 \times 10^{-3}}{1}$$

=  $9.77 \times 10^{-4}$  moles of  $\text{H}^+$  ions

Now, we know that  
 $\text{pH} = -\log_{10} [\text{H}^+]$   
 $\Rightarrow \text{pH} = -\log_{10} (9.77 \times 10^{-4})$   
 $= -\log_{10} 9.77 + (-\log_{10}(10^{-4}))$   
 $= -\log_{10} 9.77 + 4 \log_{10} 10$   
 $= -0.989 + 4$   
 $\Rightarrow \text{pH} = 3.01$

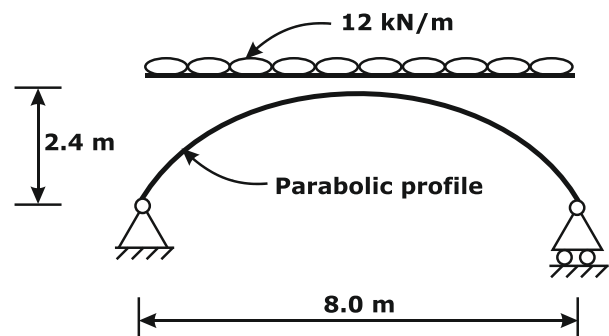
7. The Los Angeles test for stone aggregates is used to examine
- A. Soundness  
B. Abrasion resistance  
C. Specific gravity  
D. Crushing strength

**Ans.** B

**Sol.** Los Angeles test is done to check the abrasion resistance of coarse aggregate as per IS:2386 (Part IV)-1963.

Specific gravity of coarse aggregate \_\_\_\_\_  
 Using wire basket equipment, using IS:2386  
 Crushing strength deals with resistance to compressive action of aggregate  
 Soundness is a test to judge the durability of stone aggregate against weathering actions

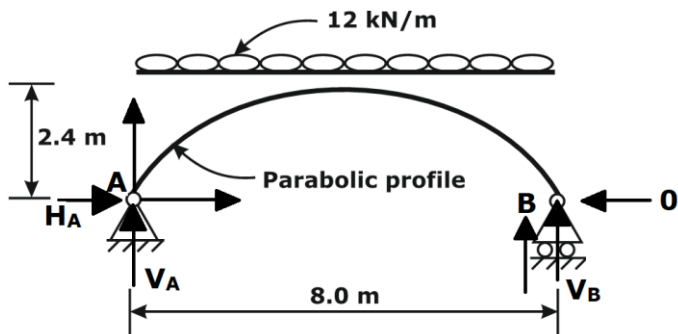
8. A planar elastic structure is subjected to uniformly distributed load, as shown in the figure (not drawn to the scale)



Neglecting self-weight, the maximum bending moment generated in the structure (in kN.m, round off to the nearest integer), is \_\_\_\_.

**Ans.** 96

**Sol.**



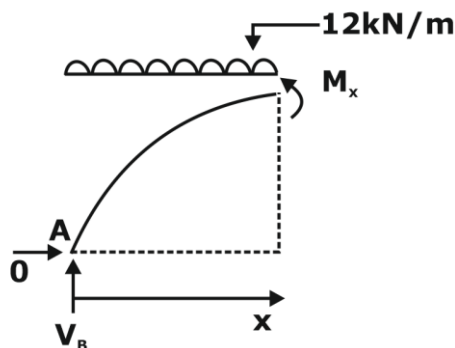
$$\sum F_x = 0 \Rightarrow H_A = 0$$

Neglecting self weight, the maximum bending moment. Taking 'A' as the origin and springing points 'A' and 'B' are at the same level.

Applying,  $\sum M_A = 0$  to the FBD of entire arch.

$$\Rightarrow 12 \times 8 \times \left(\frac{8}{L}\right) - v_B[8] = 0$$

$$\Rightarrow v_B = 48 \text{ kN}$$



$$M_x + 12x \left(\frac{x}{2}\right) - v_B[x] = 0$$

$$M_x = v_B[x] - 6[x^2]$$

$$\Rightarrow M_x = 48(x) - 6(x^2)$$

For max B.M

$$\frac{dM_x}{dx} = 0$$

$$\Rightarrow 48 - 12 \times 20 \Rightarrow x = 4 \text{ m}$$

$$(M_x)_{\max} = 48(4) - 6(4)^2 = 96 \text{ kN-m}$$

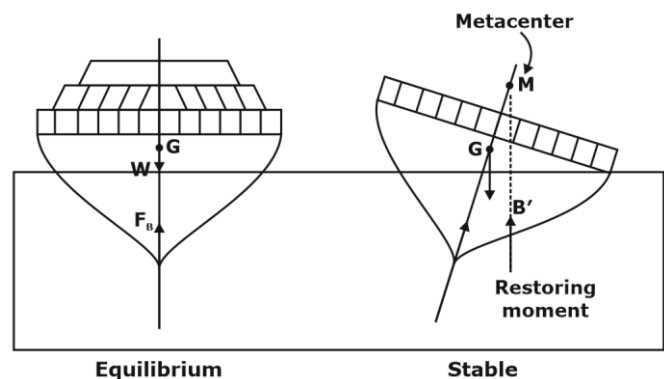
9. A body floating in a liquid is in a stable state of equilibrium if its

- Metacentre coincides with its Centre of gravity
- Metacentre lies below its centre of gravity
- Metacentre lies above its centre of gravity
- Centre of gravity is below its centre of buoyancy

**Ans.** C

**Sol.** A measure of stability for floating bodies is the metacentric height GM, which is the distance between centre of gravity G and the metacentre M.

A floating body is stable if point M is above G, and thus GM is positive.



10. A river has a flow of 1000 million litres per day (MLD). BOD<sub>5</sub> of 5 mg/litre and Dissolved Oxygen (DO) level of 8 mg/litre before receiving the wastewater discharge at a location. For the existing environmental conditions, the saturation DO level is 10 mg/litre in the river. Wastewater discharge of 100 MLD with the BOD<sub>5</sub> of 200 mg/litre and DO level of 2mg/litre falls at that location. Assuming complete mixing of wastewater and river water, the immediate DO deficit (in mg/litre, round off to two decimal places), is \_\_\_\_.

**Ans.** 2.545

**Sol.** For river,

$$\text{flow rate} = Q_R = 1000 \text{ MLD}$$

$$\text{BOD}_5 = 5 \text{ mg/l}$$

$$\text{Dissolved oxygen} = \text{DO}_R = 8 \text{ mg/l}$$

For waste water,

$$\text{Flow rate} = Q_W = 100 \text{ MLD}$$

$$\text{BOD}_5 = 200 \text{ mg/l}$$

$$\text{Dissolved oxygen} = \text{DO}_W = 2 \text{ mg/l}$$

$$\text{DO}_{\text{mix}} = \frac{\text{DO}_R \times Q_R + \text{DO}_W \times Q_W}{Q_R + Q_W}$$

$$\Rightarrow \text{DO}_{\text{mix}} = \frac{2 \times 100 + 8 \times 1000}{100 + 1000}$$

$$= 7.45 \text{ mg/l}$$

$$\text{Now, } \text{DO}_{\text{def}} = \text{DO}_{\text{sat}} - \text{DO}_{\text{mix}}$$

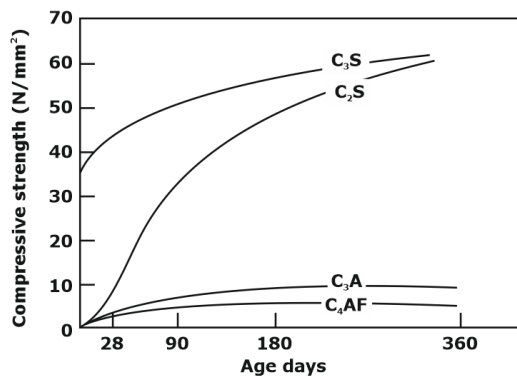
$$= 10 - 7.45 = 2.545 \text{ mg/l}$$

**11.** During the process of hydration of cement, due to increase in Dicalcium Silicate ( $\text{C}_2\text{S}$ ) content in cement clinker, the heat of hydration

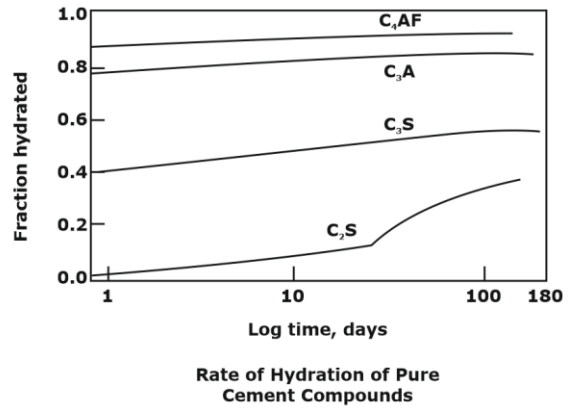
- A. Does not change
- B. Initially decreases and then increases
- C. Decreases
- D. Increases

**Ans.** B

**Sol.**



Contribution of Cement Compounds to Strength of Cement



Due to increase in  $\text{C}_2\text{S}$  content, early age strength of cement is reduced indicating @ early ages like till 7 to 14 days,

The evolution of heat of hydration is less @ early ages. But increase in  $\text{C}_2\text{S}$  content contribute to later age strength i.e., rate of gain of strength in more @ later ages (after 7 to 14 days), indicating increase in heat of hydration at later ages.

**12.** The data for an agricultural field for a specific month are given below:

$$\text{Pan Evaporation} = 100 \text{ mm}$$

$$\text{Effective Rainfall} = 20 \text{ mm (after deducting losses due to runoff and deep percolation)}$$

$$\text{Crop Coefficient} = 0.4$$

$$\text{Irrigation Efficiency} = 0.5$$

The amount of irrigation water (in mm) to be applied to the field in that month, is

- A. 10
- B. 20
- C. 80
- D. 40

**Ans.** D

$$\text{Sol. Effective rainfall} = P_{\text{eff}} = 20 \text{ mm}$$

$$\text{Water requirement} = \text{pan evaporation} \times \text{crop coefficient} = 100 \times 0.4 = 40 \text{ mm}$$

$$\therefore \text{Total additional water requirement}$$

$$= 40 - 20 = 20 \text{ mm}$$

Taking efficiency into consideration, we get the

$$\text{requirement} = \frac{20}{0.5} = 40 \text{ mm}$$

**13.** The true value of  $\ln(2)$  is 0.69. If the value of  $\ln(2)$  is obtained by linear interpolation between  $\ln(1)$  and  $\ln(6)$ , the percentage of absolute error (round off

- A. 84                                      B. 69  
C. 48                                      D. 35

**Ans. C**

**Sol.** T.V = 0.69

$$\ln_1 = 0$$

$$\ln_6 = 1.79$$

from interpolating ( $\ln_1$  &  $\ln_6$ ) we get = 0.358

(mv)

$$\%Error = \frac{T.v - mv}{T.v} \times 100$$

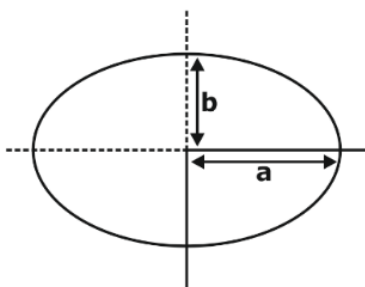
$$\%Error = 48.11\%$$

**14.** The area of an ellipse represented by an equation  $\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$  is

- A.  $\frac{\pi ab}{4}$                                       B.  $\frac{4\pi ab}{3}$   
C.  $\pi ab$                                       D.  $\frac{\pi ab}{2}$

**Ans. C**

**Sol.** Equation of ellipse is  $\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$

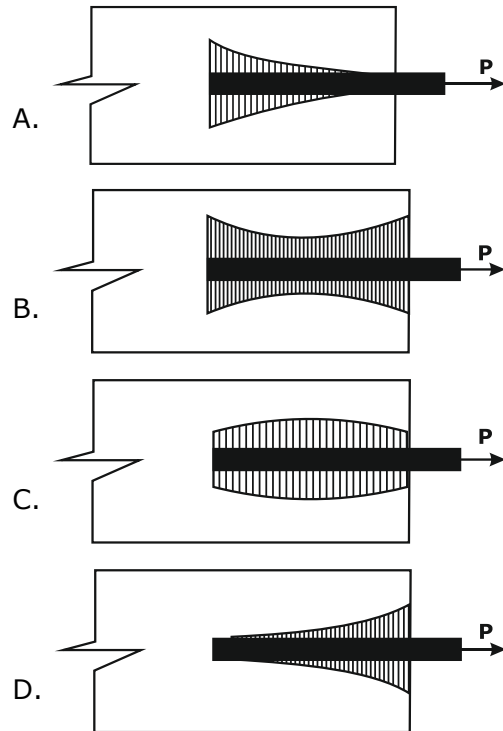


Major axis = 2a

Minor axis = 2b

Area of ellipse for standard equation is  $\pi ab$ .

**15.** A reinforcing steel bar, partially embedded in concrete, is subjected to a tensile force P. The figure that appropriately represents the distribution of the magnitude of bond stress (represented as hatched region), along the embedded length of the bar, is



**Ans. D**

**Sol.** As per IS: 456-2000 bond strength varies parabolically, near the applied load is more and away from the applied load is less.

**16.** Which one of the following statements is NOT correct?

- A. In case of a point load. Boussinesq's equation predicts higher value of vertical stress at a point directly beneath the load as compared to Westergaard's equation.  
B. The cohesion of normally consolidated clay is zero when triaxial test is conducted under consolidated undrained condition.



- C. The ultimate bearing capacity of a strip foundation supported on the surface of sandy soil increases in direct proportion to the width of footing.
- D. A clay deposit with a liquidity index greater than unity is in a state of plastic consistency.

**Ans.** D

**Sol.** For  $IL > 1$  is in under liquid condition not plastic.

- 17.** In a soil investigation work at a site, Standard Penetration Test (SPT) was conducted at every 1.5 m interval up to 30 m depth. At 3 m depth, the observed number of hammer blows for three successive 150 mm penetrations were 8, 6 and 9, respectively. The SPT N-value at 3m depth is
- A. 15                              B. 23  
C. 17                              D. 14

**Ans.** A

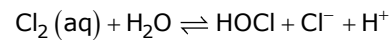
**Sol.** Blows for first 150 mm is not noted. Thereafter for next 300 mm penetration number of blows are counted.  
 $\therefore$  SPT value =  $9 + 6 = 15$

- 18.** In an urban area, a median is provided to separate the opposing streams of traffic. As per IRC : 86-1983, the desirable minimum width (in m, expressed as integer) of the median, is \_\_\_\_.

**Ans.** 3-5

**Sol.** As per IRC, for urban area the width of median varies from 0.9 m to 5 m. whereas for rural areas, the width varies from 3 m to 5m.

- 19.** During chlorination process, aqueous (aq) chlorine reacts rapidly with water to form  $Cl^-$ , HOCl, and  $H^+$  as shown below



The most active disinfectant in the chlorination process from amongst the following, is

- A. HOCl                              B.  $H^+$   
C.  $H_2O$                               D.  $Cl^-$

**Ans.** A

**Sol.** HOCl is 80 times more active than  $OCl^-$  as it is very unstable. The amount or sum of HOCl and  $OCl^-$  is known as free available chlorine.

- 20.** In a drained triaxial compression test, a sample of sand fails at deviator stress of 150 kPa under confining pressure of 50 kPa. The angle of internal friction (in degree, round off to the nearest integer) of the sample is

**Ans.**  $36.86^\circ$

**Sol.**       $\sigma_3 = 50$

$$\sigma_1 = 200(50 + 150)$$

We know that

$$\sigma_1 = \sigma_3 \left( \frac{1 + \sin \phi}{1 - \sin \phi} \right) + 2C \sqrt{\frac{1 + \sin \phi}{1 - \sin \phi}}$$

For sand  $C = 0$

$$200 = 50 \left( \frac{1 + \sin \phi}{1 - \sin \phi} \right)$$

$$4 = \frac{1 + \sin \phi}{1 - \sin \phi}$$

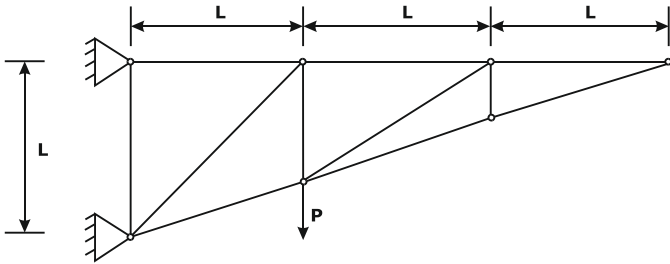
$$4 - 4\sin \phi = 1 + \sin \phi$$

$$5 \sin \phi = 3$$

$$\phi = \sin^{-1} \left( \frac{3}{5} \right)$$

$$\phi = 36.86^\circ$$

21. Consider the planar truss shown in the figure (not drawn to the scale)

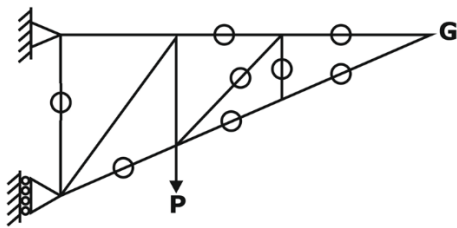


Neglecting self-weight of the members, the number of zero-force members in the truss under the action of the load P, is

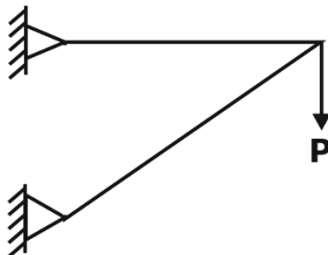
- A. 7
- B. 9
- C. 6
- D. 8

Ans. A

Sol. Using Golden Rules -1 & 2,

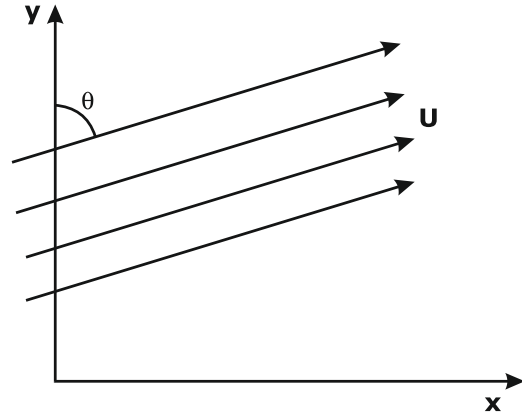


No. of zero force members = 8  
Idealized structure



No. of zero force members are 8.  
Using golden rules 1 and 2 we can find 0 forces.  
No. of zero force members are "8"  
As displacement between "A" & "B" points in vertical direction is = 0, i.e.  $\Delta_{AB} = 0$ ,  
Resisting force =  $F_{AB} = 0$

22. Uniform flow with velocity U makes an angle  $\theta$  with the y-axis, as shown in the figure



The velocity potential ( $\phi$ ), is

- A.  $\pm U (x \sin\theta - y \cos\theta)$
- B.  $\pm U (y \sin\theta + x \cos\theta)$
- C.  $\pm U (x \sin\theta + y \cos\theta)$
- D.  $\pm U (y \sin\theta - x \cos\theta)$

Ans. C

Sol. We know that,  $u_x = \frac{-\partial\phi}{\partial x}$

$$u_y = \frac{-\partial\phi}{\partial y}$$

velocity in x-direction,  $u_x = u \sin\theta$   
velocity in y-direction,  $u_y = u \cos\theta$   
Now,

$$\frac{-\partial\phi}{\partial x} = u_x \Rightarrow \frac{-\partial\phi}{\partial x} = u \sin\theta$$

Integrating above equation, we get

$$\phi = -u \sin\theta x + f(y) + c \rightarrow (1)$$

Similarly

$$\phi = -u \cos\theta y + f(x) + c \rightarrow (2)$$

From equation (1) and (2), we get

$$\phi = -u (x \sin\theta + y \cos\theta)$$

when,  $\frac{\partial\phi}{\partial x} = u_x$  and  $\frac{\partial\phi}{\partial y} = u_y$

$$\phi = u (x \sin\theta + y \cos\theta)$$

$$\therefore \phi = \pm u (x \sin\theta + y \cos\theta)$$

23. Velocity of flow is proportional to the first power of hydraulic gradient in Darcy's law. This is law is applicable to

- A. Turbulent flow in porous media
- B. Transitional flow in porous media
- C. Laminar flow in porous media
- D. Laminar as well as turbulent flow in porous media

**Ans. C**

**Sol.** The simplest form of Darcy's law states that

$$v = \frac{Q}{A} = -K \frac{\partial h}{\partial l}$$

Since the velocity in laminar flow is proportional to the first power of the hydraulic gradient (Poiseuille's law), it is reasonable to apply Darcy's law to laminar flow in porous media.

- 24.** In the following partial differential equation,  $\theta$  is a function of  $t$  and  $z$ . and  $D$  and  $K$  are functions of  $\theta$

$$D(\theta) \frac{\partial^2 \theta}{\partial z^2} + \frac{\partial K(\theta)}{\partial z} - \frac{\partial \theta}{\partial t} = 0$$

The above equation is

- A. A second order linear equation
- B. A second-degree non-linear equation
- C. A second order non-linear equation
- D. A second-degree linear equation

**Ans. C**

- 25.** A road in a hilly terrain is to be laid at a gradient of 4.5%. A horizontal curve of radius 100 m is laid at a location on this road. Gradient needs to be eased due to combination of curved horizontal and vertical profiles of the road. As per IRC, the compensated gradient (in %, round off to one decimal place), is \_\_\_\_.

**Ans. 4**

**Sol.** According to IRC

$$\text{Grade compensation} = \left. \frac{30 + R}{R} \right\} \frac{75}{R} \Bigg\}_{\text{minm.}}$$

$$\text{Now, } \frac{30 + 100}{100} = 1.3\%$$

$$\frac{75}{100} = 0.75\%$$

$$\text{Compensated grade} = 4.5 - 0.75 = 3.75\%$$

But, according to IRC the minimum value of compensated grade is 4%. Therefore answer is 4%.

- 26.** Traffic volume count has been collected on a 2-lane road section which needs upgradation due to severe traffic flow condition. Maximum service flow rate per lane is observed as 1280 veh/h at level of service "C". The Peak Hour Factor is reported as 0.78125. Historical traffic volume count provides Annual Average Daily Traffic as 12270 veh/day. Directional split of the traffic flow is observed to be 60:40. Assuming that traffic stream consists of "All Cars" and all drivers are 'Regular Commuters', the number of extra lane(s) (round off to the next higher integer) to be provided, is \_\_\_\_.

**Ans. 6**

**Sol.** Given,

$$\text{Peak hour factor} = \text{PHF} = 0.78125$$

$$\text{Maximum service flow rate of LOS}$$

$$= \text{MSF} = 1280$$

$$F_{HV} = 1$$

$$\text{Road under familiarity adjustment ejector}$$

$$= f_p = 1$$

Now, we know that, number of lane (N)

$$N = \frac{\text{DDHV}}{\text{PHF} \times \text{MSF} \times F_{HV} \times f_p}$$

Here, DDHV = Directional distribution hour volume.

$$\text{DDHV} = 122270 \times 0.6 = 7362$$

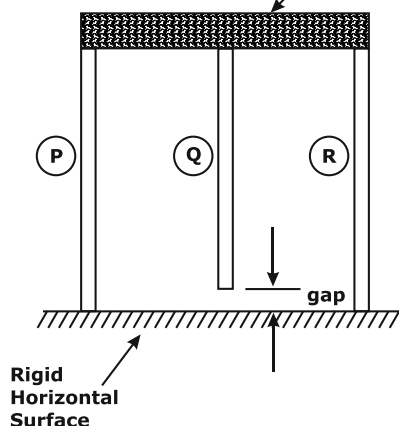
$$\therefore N = \frac{7362}{0.78125 \times 1280 \times 1 \times 1}$$

$$= 7.362 = 8 \text{ lanes}$$

Number of extra lanes =  $8 - 2 = 6$  lanes.

- 27.** A rigid, uniform, weightless, horizontal bar is connected to three vertical members P, Q and R as shown in the figure (not drawn to the scale). All three members have identical axial stiffness of 10 kN/mm. The lower ends of bar P and R rest on a rigid horizontal surface. When NO load is applied, a gap of 2 mm exists between the lower end of the bar Q and the rigid horizontal surface. When a vertical load W is placed on the horizontal bar in the downward direction, the bar still remains horizontal and gets displaced by 5 mm in the vertically downward direction.

Rigid Uniform Weightless Horizontal Bar

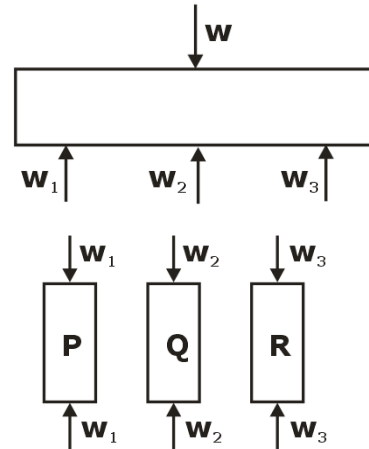


The magnitude of the load W (in kN, round off to the nearest integer), is

**Ans.** 130

**Sol.**

$$\frac{AE}{L} = 10 \text{ kN/mm}$$



$$w_1 + w_2 + w_3 = W$$

from symmetry  $\Rightarrow w_1 = w_3$

$$\delta_P = 5 \text{ mm} = \frac{w_1 L}{AE}$$

$$\therefore w_1 = 50 \text{ kN} = w_3$$

$$\delta_Q = \frac{w_2 L}{AE}$$

$$\therefore w_2 = 30 \text{ kN}$$

$$\therefore W = 130 \text{ kN}$$

- 28.** In a homogeneous unconfined aquifer of area 3.00 km<sup>2</sup>, the water table was at an elevation of 102.00 m. After a natural recharge of volume 0.90 million cubic meter (Mm<sup>3</sup>), the water table rose to 103.20 m. After this recharge, ground water pumping took place and the water table dropped down to 101.20 m. The volume of ground water pumped after the natural recharge, expressed (in Mm<sup>3</sup> and round off to two

**Ans.** 1.5

**Sol.** Volume of water coming =  $0.9 \times 10^6 \text{ m}^3$

$$\text{Height of water} = \frac{0.9 \times 10^6}{3 \times 10^6} = 0.3 \text{ m}$$

$$n = \text{Porosity} = \frac{V_V}{V_T}$$

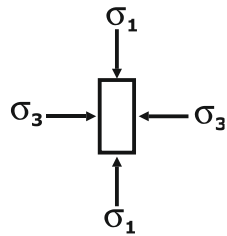
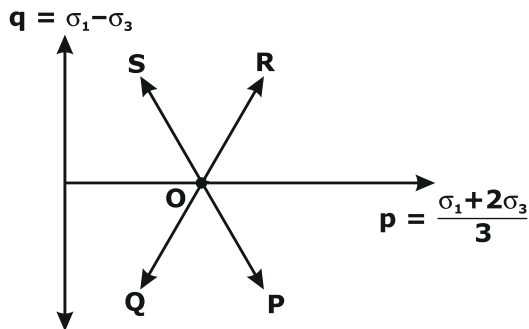
$$n = \frac{0.3}{1.2} = 0.25$$

Now pumping

Volume = Area × Height

$$= 3 \times 10^6 \times 2 \times 0.25 = 1.5 \times 10^6 \text{ m}^3$$

29. The total stress paths corresponding to different loading conditions, for a soil specimen under the isotropically consolidated stress state (O), are shown below



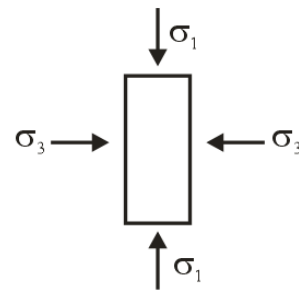
Stress Path	Loading Condition
OP	I-Compression loading ( $\sigma_1$ - increasing; $\sigma_3$ - constant)
OQ	II-Compression unloading ( $\sigma_1$ - constant; $\sigma_3$ - decreasing)
OR	III- Extension unloading ( $\sigma_1$ - decreasing; $\sigma_3$ - constant)
OS	IV - Extension loading ( $\sigma_1$ - constant; $\sigma_3$ - increasing)

The correct match between the stress paths and the listed loading conditions, is

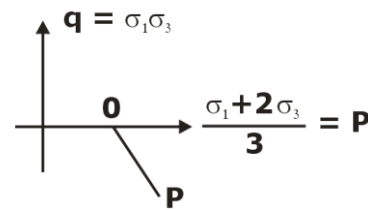
- A. OP - IV, OQ - III, OR- I, OS - II
- B. OP - III, OQ - II, OR - I, OS - IV
- C. OP - I, OQ - III, OR - II, OS - IV
- D. OP - I, OQ - II, OR - IV, OS - III

Ans. A

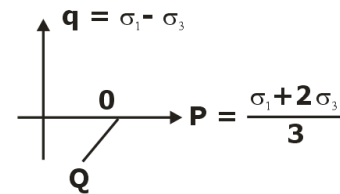
Sol.



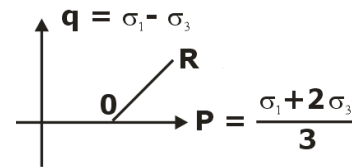
$\sigma_1 \text{ const } \sigma_3 \uparrow \rightarrow y \text{ coord } \downarrow \text{ \& } x \uparrow$



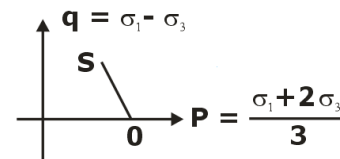
$\sigma_1 \downarrow \text{ \& } \sigma_3 = \text{const} \rightarrow y \text{ axis } \downarrow \text{ \& } x \downarrow$



$\sigma_1 \uparrow \text{ \& } \sigma_3 = \text{const} = x \text{ axis } \uparrow \text{ \& } y \uparrow$



$\sigma_1 \text{ const } \sigma_3 \downarrow \rightarrow y \text{ axis } \uparrow \text{ \& } y \downarrow$



30. A continuous function/ $f(x)$  is defined. If the third derivative at  $x$ , is to be computed by using the fourth order central finite-difference scheme (with step length =  $h$ ), the correct formula is

$$A. f'''(x_i) = \frac{f(x_{i+3}) - 8f(x_{i+2}) + 13f(x_{i+1}) + 13f(x_{i-1}) - 8f(x_{i-2}) - f(x_{i-3})}{8h^3}$$

$$B. f'''(x_i) = \frac{-f(x_{i+3}) - 8f(x_{i+2}) - 13f(x_{i+1}) + 13f(x_{i-1}) + 8f(x_{i-2}) - f(x_{i-3})}{8h^3}$$

$$C. f'''(x_i) = \frac{f(x_{i+3}) - 8f(x_{i+2}) - 13f(x_{i+1}) + 13f(x_{i-1}) + 8f(x_{i-2}) + f(x_{i-3})}{8h^3}$$

$$D. f'''(x_i) = \frac{-f(x_{i+3}) + 8f(x_{i+2}) - 13f(x_{i+1}) + 13f(x_{i-1}) - 8f(x_{i-2}) + f(x_{i-3})}{8h^3}$$

**Ans. D**

**31.** A gaseous chemical has a concentration of  $41.6 \mu\text{mol}/\text{m}^3$  in air at 1 atm pressure and temperature 293 K. The universal gas constant  $R$  is  $82.05 \times 10^{-6} (\text{m}^3 \text{atm})/(\text{mol K})$ . Assuming that ideal gas law is valid, the concentration of the gaseous chemical (in ppm, round off to one decimal place), is \_\_\_\_.

**Ans. 1**

**Sol.** We know that,

$$PV = nRt$$

Where,  $P$  = Pressure

$V$  = Volume

$n$  = number of moles

$R$  = Universal gas constant

$T$  = Temperature

$$\text{So, } V = \frac{nRT}{P} = \frac{41.6 \times 10^{-6} \times 82.05 \times 10^{-6} \times 293}{1}$$

$$\Rightarrow V = 10^{-6} \text{ m}^3$$

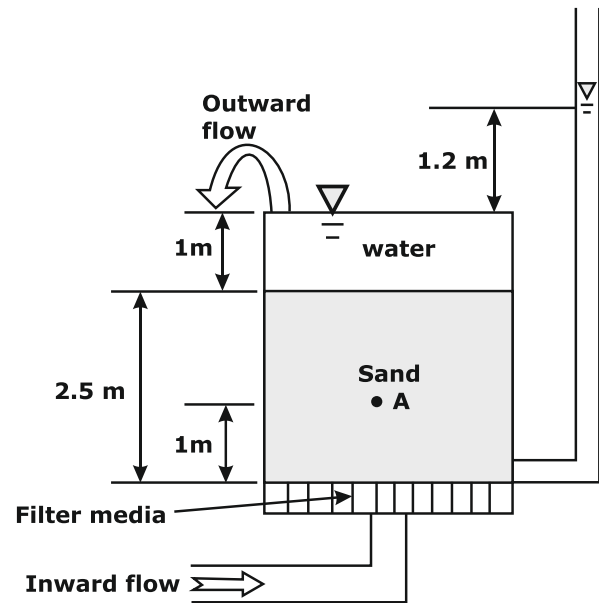
$$1 \text{ ppm} = \frac{1 \text{ part of gas}}{10^6 \text{ parts of air}} = \frac{1 \text{ m}^3 \text{ of gas}}{10^6 \text{ m}^3 \text{ of air}}$$

$$\Rightarrow 1 \text{ ppm} = \frac{41.6 \times 10^{-6} - 4 \text{ moles}}{10^6 \text{ cm}^3}$$

Since,  $41.6 - 4$  mole of gas volume of  $10^{-6} \text{ m}^3$

$$\therefore 41.6 - 4 \text{ moles}/\text{m}^3 = 1 \text{ ppm}$$

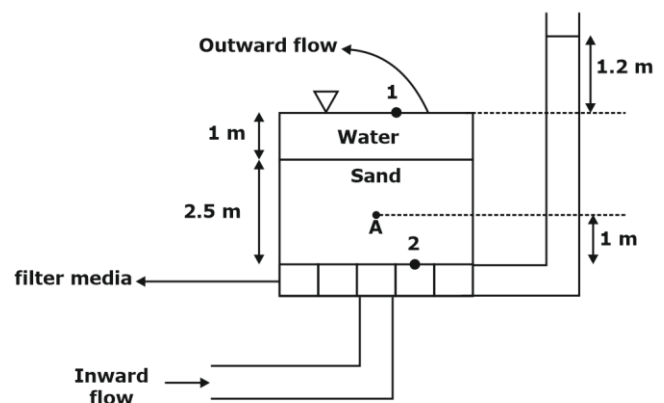
**32.** Water flows in the upward direction in a tank through 2.5 m thick sand layer as shown in the figure. The void ratio and specific gravity of sand are 0.58 and 2.7, respectively. The sand is fully saturated. Unit weight of water is  $10 \text{ kN}/\text{m}^3$ .



The effective stress (in kPa, round off to two decimal places) at point A, located 1 m above the base of tank, is

**Ans. 8.925 kPa**

**Sol.**



Taking 2 as datum

	PH	VH	DH	TH
2	4.7	0	0	4.7
1	0	0	3.5	3.5
A	x	0	1	$4.7 - 0.48 = 4.22$

$$x + 0 + 1 = 4.22$$

$$x = 3.22$$

$$i = \frac{hc}{c} = \frac{1.2}{2.5} = .48$$

$$\bar{\sigma}_A = \sigma - u$$

$$\bar{\sigma}_A = 8.925 \text{ kN/m}^3$$

**33.** For the Ordinary Differential Equation

$$\frac{d^2x}{dt^2} - 5 \frac{dx}{dt} + 6x = 0, \text{ with initial conditions}$$

$$x(0) = 0 \text{ and } \frac{dx}{dt}(0) = 10, \text{ the solution is}$$

A.  $-10e^{2t} + 10e^{3t}$

B.  $10e^{2t} + 10e^{3t}$

C.  $5e^{2t} + 6e^{3t}$

D.  $-5e^{2t} + 6e^{3t}$

**Ans. A**

**Sol.**  $\frac{d^2x}{dt^2} - 5 \frac{dx}{dt} + 6x = 0$

$$D^2 - 5D + 6 = 0$$

$$D^2 - 3D - 2D + 6 = 0$$

$$D(D - 3) - 2(D - 3) = 0$$

$$D = 2, 3$$

Solution will be,  $x = C_1e^{3t} + C_2e^{2t}$

Applying boundary condition

$$x(0) = 0$$

$$C_1 + C_2 = 0 \rightarrow (1)$$

$$\frac{dx}{dt} = 3C_1e^{3t} + 2C_2e^{2t}$$

$$\frac{dx}{dt}(0) = 10$$

$$10 = 3c_1 + 2c_2 \rightarrow (2)$$

Form equation (1) and (2)

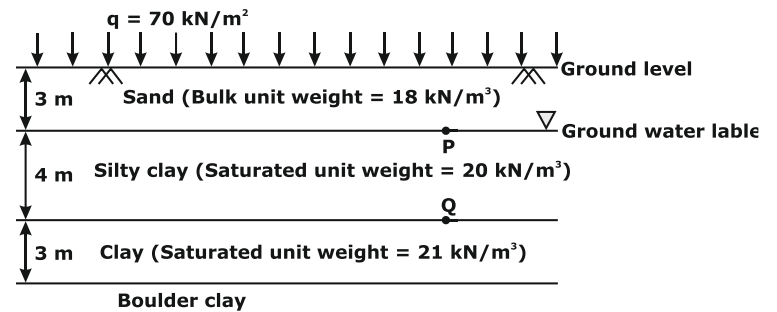
$$C_1 = 10, C_2 = -10$$

So, final solution becomes,  $x = 10e^{3t} - 10e^{2t}$

Or

$$x = -10e^{2t} + 10e^{3t}$$

**34.** The soil profile at a site up to a depth of 10 m is shown in the figure (not drawn to the scale). The soil is preloaded with a uniform surcharge ( $q$ ) of  $70 \text{ kN/m}^2$  at the ground level. The water table is at a depth of 3 m below ground level. The soil unit weight of the respective layers is shown in the figure. Consider unit weight of water as  $9.81 \text{ kN/m}^3$  and assume that the surcharge ( $q$ ) is applied instantaneously.



Immediately after preloading, the effective stresses (in kPa) at points P and Q, respectively, are

A. 54 and 95

B. 36 and 90

C. 36 and 126

D. 124 and 204

**Ans. A**

**Sol.** Surcharge is applied instantaneous

$\therefore$  Extra pore water pressure of 7 kPa is devalated.

$$\bar{\sigma}_p = \sigma_p - v_p$$

$$\sigma_p = 70 + 18 \times 3 = 124$$

$$u_p = 0 + 70 = 70$$

$$\bar{\sigma}_p = 124 - 70 = 54$$

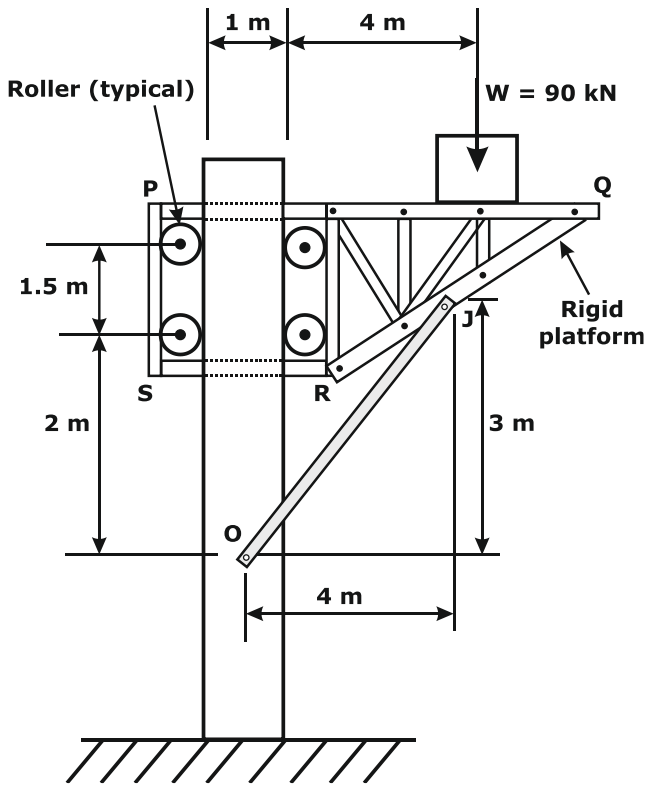
$$\bar{\sigma}_q = \sigma_q - v_q$$

$$\sigma_q = 70 + 18 \times 3 + 20 \times 4 = 204$$

$$v_q = 9.81 \times 4 + 70 = 109.24$$

$$\bar{\sigma}_p = 204 - 109.24 = 94.76 \text{ kPa}$$

**35.** A rigid weightless platform PQRS shown in the figure (not drawn to the scale) can slide freely in the vertical direction. The platform is held in position by the weightless member OJ and four weightless, frictionless rollers, Points O and J are pin connections. A block of 90 kN rests on the platform as shown in the figure

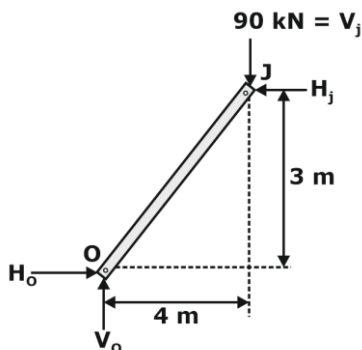


The magnitude of horizontal component of the reaction (in kN) at pin O, is

- A. 90                                      B. 120  
C. 150                                      D. 180

**Ans. B**

**Sol.** Since the vertical load is resisted by bar OJ only



FBD of OJ

$$\Sigma MJ = 0$$

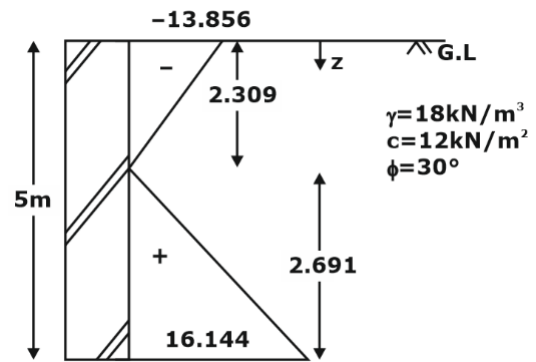
$$H_o \times 3 + 90 \times 4 = 0$$

$$H_o = 120 \text{ kN}$$

**36.** A vertical retaining wall of 5 m height has to support soil having unit weight of  $18 \text{ kN/m}^3$ , effective cohesion of  $12 \text{ kN/m}^2$ , and effective friction angle of  $30^\circ$ . As per Rankine's earth pressure theory and assuming that a tension crack has occurred, the lateral active thrust on the wall per meter length (in kN/m, round off to two decimal places), is

**Ans.** 21.72 kw/m

**Sol.**



$$k_a = \frac{1 - \sin 30}{1 + \sin 30} = \frac{1 - .5}{1 + .5} = \frac{.5}{1.5} = 1/3$$

$$\text{Depth of tension crack } \frac{2c}{\gamma \sqrt{k_a}} = \frac{2 \times 12}{18 \sqrt{1/3}} = 2.309$$

$$\sigma_H = k_a \sigma_v - 2c \sqrt{k_a}$$

$$\sigma_H = \frac{1}{3} \times 18 \times z - 2 \times 12 \times \sqrt{\frac{1}{3}}$$

$$\sigma_H = 6z - 13.856$$

$$\sigma_H \text{ AT TOP (z = 0) = - 13.856}$$

$$\sigma_H \text{ AT BOTTOM (z = 5) = 16.144}$$

$$\text{Net thrust} = \left[ \frac{0 + 16.144}{2} \right] \times 2.69 \times 1$$

$$= 21.72 \text{ kw/m}$$



**37.** Surface Overflow Rate (SOR) of a primary settling tank (discrete settling) is 20000 litre/m<sup>2</sup> per day. Kinematic viscosity of water in the tank is  $1.01 \times 10^{-2}$  cm<sup>2</sup>/s. Specific gravity of the settling particles is 2.64. Acceleration due to gravity is 9.81 m/s<sup>2</sup>. The minimum diameter (in  $\mu\text{m}$ , round off to one decimal place) of the particles that will be removed with 80% efficiency in the tank, is .

**Ans.** 14.46

**Sol.** According to stokes law,

$$V_s = \frac{(4-1)gc^2}{18v}$$

$$\text{Also, } \eta = 80 = \frac{u_s}{v_s} \times 100$$

Here,  $v_s = 20000 \text{ l/m}^2/\text{day}$   
 = surface over flow rate

$$\Rightarrow u_s = \frac{0.8 \times 20000 \times 10^{-3}}{86400}$$

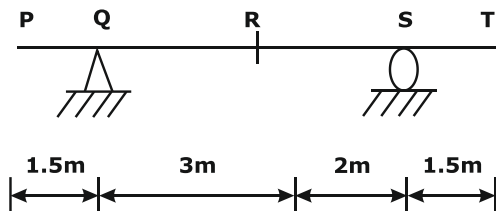
$$= 1.85 \times 10^{-4} \text{ m/sec}$$

$$\therefore 1.85 \times 10^{-4} = \frac{(2.64-1)9.81 \times d^2}{18 \times 1.01 \times 10^{-2} \times 10^{-4}}$$

$$\Rightarrow d = 1.446 \times 10^{-5} \text{ m}$$

$$\Rightarrow d = 14.46 \times 10^{-6} \mu\text{m}$$

**38.** Distributed load (s) of 50 kN/m may occupy any position(s) (either continuously or in patches) on the girder PQRST as shown in the figure (not drawn to the scale)

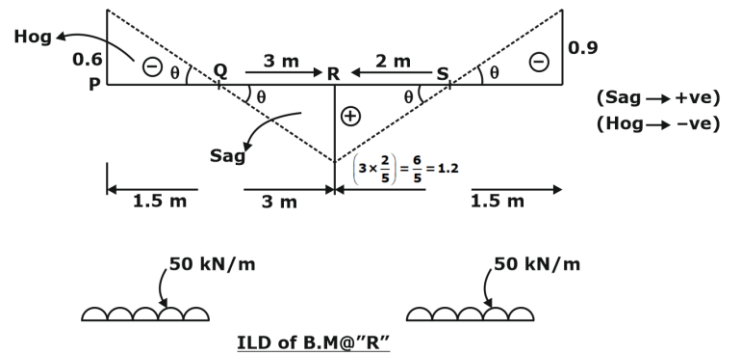


The maximum negative (hogging) bending moment (in kN.m) that occurs at point R, is

- A. 56.25                      B. 150.00  
 C. 93.75                      D. 22.50

**Ans.** A

**Sol.**



Maximum hogging moment at "R" is possible if the UDL is loaded on over hang spans (PQ & ST)

Magnitude of Hogging moment

$$= 50 \times \left\{ -\frac{1}{2} \times 1.5 \times 0.6 \right\} + 50 \times \left\{ -\frac{1}{2} \times 1.5 \times 0.9 \right\}$$

$$= -(0.45 + 0.675) \times 50$$

$$= - 56.25 \text{ kN-m (Hog)}$$

**39.** A stream with a flow rate of 5 m<sup>3</sup>/s is having an ultimate BOD of 30 mg/litre. A wastewater discharge of 0.20 m<sup>3</sup>/s having BOD<sub>5</sub> of 500 mg/litre joins the stream at a location and instantaneously gets mixed up completely. The cross-sectional area of the stream is 40 m<sup>2</sup> which remains constant. BOD exertion rate constant is 0.3 per day (logarithm base to e). The BOD (in mg/litre, round off to two decimal places) remaining at 3 km downstream from the mixing location, is .

**Ans.** 49.57

**Sol.** We know that

$$L_1 = L_0 e^{-k \times t}$$

$L_0$  = Dissolved oxygen of  $m_i = DO_{mix}$

$$DO_{mix} = \frac{Q_R BOD_{UR} + Q_S \cdot BOD_U}{Q_S + Q_R}$$

Here,  $Q_S$  = flow rate of sewage

$Q_R$  = flow rate of river.

For sewage

Also,  $BOD_s = BOD_u (1 - e^{-5k})$

$$\Rightarrow BOD_o = \frac{500}{1 - e^{-0.3 \times 5}}$$

$$= 643.66 \text{ mg/l}$$

$$DO_{mix} = \frac{5 \times 30 + 0.2 \times 643.66}{5 + 0.2}$$

$$DO_{mix} = 53.6 \text{ mg/l}$$

$$L_x = 53.6 e^{-0.3 \times 0.26}$$

$$L_x = 49.57 \text{ mg/l}$$

- 40.** A water supply scheme transports 10 MLD (Million Litres per Day) water through a 450 mm diameter pipeline for a distance of 2.5 km. A chlorine dose of 3.50 mg/litre is applied at the starting point of the pipeline to attain a certain level of disinfection at the downstream end. It is decided to increase the flow rate from 10 MLD to 13 MLD in the pipeline. Assume exponent for concentration,  $n = 0.86$ . With this increased flow, in order to attain the same level of disinfection, the chlorine dose

- A. 3.95                      B. 4.40  
C. 5.55                      D. 4.75

**Ans.** D

**Sol.** In the disinfection process we have the relationship

$$tc^n = k$$

where,  $t$  = time required to kill all organism

$c$  = concentration of disinfectant

$K$  = constant

$$\therefore t_1 c_1^n = t_2 c_2^n$$

$$\Rightarrow \text{we know, } Q = \frac{V}{t} \Rightarrow t = \frac{V}{Q}$$

$$\therefore \frac{V}{Q_1} c_1^n = \frac{V}{Q_2} c_2^n$$

$$\Rightarrow \frac{1}{10} (3.5)^{0.86} = \frac{1}{13} \times (c)^{0.86}$$

$$\Rightarrow c = 4.75 \text{ mg/l}$$

- 41.** If  $C$  represents a line segment between  $(0, 0, 0)$  and  $(1, 1, 1)$  in Cartesian coordinate system, the value (expressed as integer) of the line integral

$$\int_C [(y+z)dx + (x+z)dy + (x+y)dz] \text{ is } \underline{\hspace{2cm}}.$$

**Ans.** 3

**Sol.** Equation of a line segment

$$\frac{x}{1} = \frac{y}{1} = \frac{z}{1} = k$$

$$x = k, y = k, z = k \Rightarrow dx = dk$$

$$0 \leq x \leq 1$$

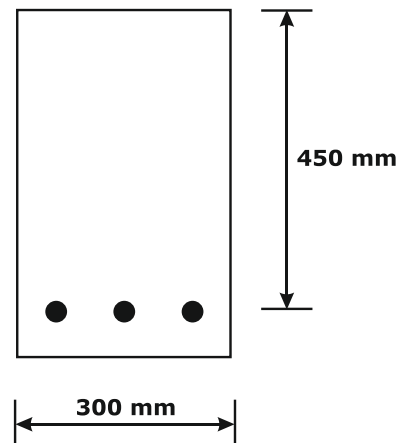
$$\therefore 0 \leq k \leq 1$$

$$\int_0^1 (2k)dk + \int_0^1 kdk + \int_0^1 2kdk$$

$$= 3 \left[ k^2 \right]_0^1$$

$$= 3$$

- 42.** The singly reinforced concrete beam section shown in the figure (not drawn to the scale) is made of M25 grade concrete and Fe500 grade reinforcing steel. The total cross-sectional area of the tension steel is 942 mm<sup>2</sup>.



As per Limit State design of IS 456-2000, the design moment capacity (in kN.m, round off to two decimal places) of the beam section, is

**Ans.** 158.277

**Sol.**  $A_{st} = 942 \text{ mm}^2$ ,  $f_{ck} = 25 \text{ N/mm}^2$

For Fe500  $\rightarrow x_{u,max} = 0.46d$

$$= 0.46 \times (450)$$

$$x_{u,max} = 207 \text{ mm}$$

Finding actual depth of neutral axis

$$C = T$$

$$0.36 f_{ck} \cdot b \cdot x_u = 0.87 f_y \cdot A_{st}$$

$$\rightarrow 0.36 \times 25 \times 300 \times x_u$$

$$= 0.87 \times 500 \times 942$$

$$x_u = 151.766 \text{ mm}$$

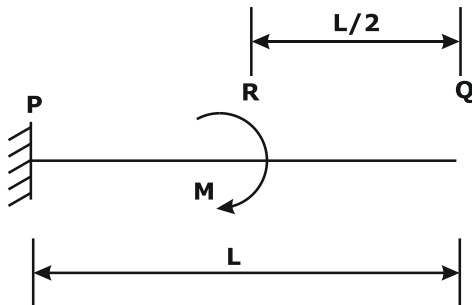
$A_s x_u < x_{u,max} \rightarrow$  The section is under reinforced section

$$M_u = M.R = 0.36 f_{ck} \cdot b \cdot x_u (d - 0.42 x_u)$$

$$= 0.36 \times 25 \times 300 \times 151.766 \times (450 - 0.42 \times 151.76)$$

$$M_u = 158.277 \text{ kN-m}$$

**43.** A cantilever beam PQ of uniform flexural rigidity (EI) is subjected to a concentrated moment M at R as shown in the figure



The deflection at the free end Q is

A.  $\frac{3ML^2}{4EI}$

B.  $\frac{3ML^2}{8EI}$

C.  $\frac{ML^2}{4EI}$

D.  $\frac{ML^2}{6EI}$

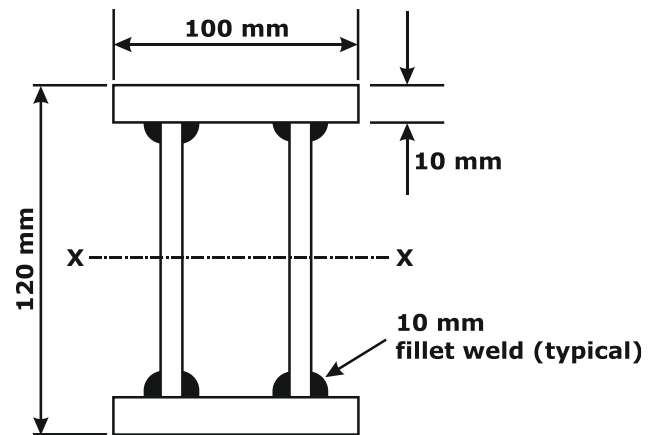
**Ans.** B

**Sol.**  $\delta_R + \theta_R \cdot \frac{L}{2}$

$$= \frac{M \left(\frac{L}{2}\right)^2}{2EI} + \frac{M \frac{L}{2}}{EI} \times \frac{L}{2}$$

$$= \frac{3 ML^2}{8 EI}$$

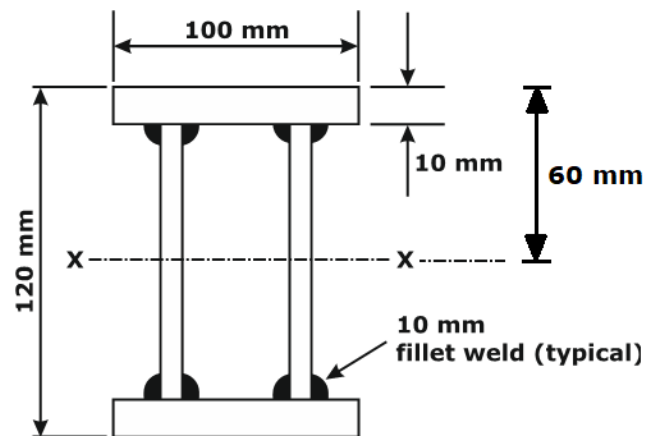
**44.** The flange and web plates of the doubly symmetric built-up section are connected by continuous 10 mm thick fillet welds as shown in the figure (not drawn to the scale). The moment of inertia of the section about its principal axis X—X is  $7.73 \times 10^6 \text{ mm}^4$ . The permissible shear stress in the fillet welds is  $100 \text{ N/mm}^2$ . The design shear strength of the section is governed by the capacity of the fillet welds.



The maximum shear force (in kN, round off to one decimal place) that can be carried by the section, is \_\_\_\_\_.

**Ans.** 393.5

**Sol.**



$$b = 4 \times \dots$$

$$b = 4 \times (0.7 \times 10)$$

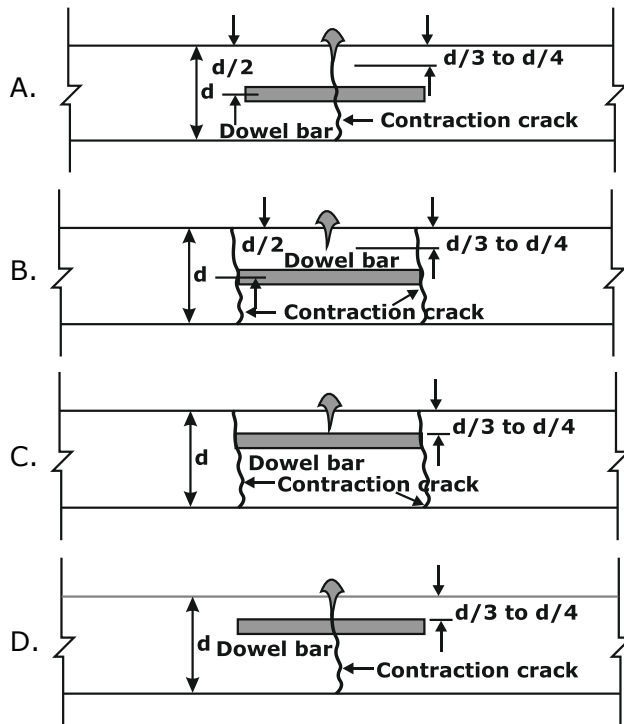
$$\text{Permissible stress in weld} = q = \frac{VA\bar{y}}{Ib}$$

$$100 = \frac{(100 \times 10) \times (60 - 5)}{7.73 \times 10^6 \times (4 \times 0.7 \times 10)}$$

$$V = 393.527 \text{ kN}$$

$$V = 393.5 \text{ kN}$$

45. A dowel bar is placed at a contraction joint. When contraction occurs, the concrete slab cracks at predetermined location (s). Identify the arrangement, which shows the correct placement of dowel bar and the place of occurrence of the contraction crack(s).



Ans. B

46. An open traverse PQRST is surveyed using theodolite and the consecutive coordinates obtained are given in the table

Lin	Consecutive Coordinates			
	Northin g (m)	Southin g (m)	Eastin g (m)	Westin g (m)
PQ	110.2	-	45.5	-
QR	80.6	-	-	60.1
RS	-	90.7	-	70.8
ST	-	105.4	55.5	-

If the independent coordinates (Northing, Easting) of station P are (400 m, 200 m), the independent coordinates (in m) of station T, are

- A. 194.7, 370.1      B. 405.3, 229.9  
C. 205.3, 429.9      D. 394.7, 170.1

Ans. D

$$\text{Sol. } \Sigma L = 190.8 - 196.1 = -5.3$$

$$\Sigma D = 101 - 130.9 = -29.9$$

$$P(400\text{m}, 200\text{m})$$

Coordinate of T are

$$= (400 - 5.3, 200 - 29.9)$$

$$= (394.7, 170.1)$$

47. Water flows at the rate of 12 m<sup>3</sup>/s in a 6 m wide rectangular channel. A hydraulic jump is formed in the channel at a point where the upstream depth is 30 cm (just before the jump). Considering acceleration due to gravity as 9.81 m/s<sup>2</sup> and density of water as 1000 kg/m<sup>3</sup>, the energy loss in the jump is
- A. 114.2 MW      B. 114.2 kW  
C. 141.2 J/s      D. 141.2 h.p.

Ans. B

Sol. Head loss in a hydraulic jump

$$= h_1 = \frac{(y_2 - y_1)^3}{4y_1y_2}$$

$$\text{Here, } y_1 = 0.3\text{m}$$

We know that,

$$y_2 = \frac{y_1}{2} \left( -1 + \sqrt{1 + 8F_1^2} \right)$$

$$\text{So, } F_1 = \left( \frac{q^2}{gy_1^3} \right)^{1/2} = \left( \frac{2^2}{(9.81 \times 0.3^3)} \right)^{1/2} = 3.88$$

$$\therefore y_2 = \frac{0.3}{2} \left[ -1 + \sqrt{1 + 8 \times 3.88^2} \right]$$

$$\Rightarrow y_2 = 1.505 \text{ m}$$

$$\text{Now, } h_2 = \frac{(1.505 - 0.3)^2}{4 \times 1.505 \times 0.3}$$

$$= 0.968 \text{ m}$$

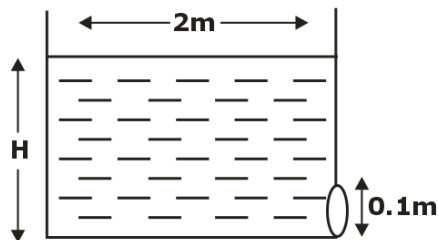
$$\text{Power lost} = r_w Q h_2 = 9.81 \times 12 \times 0.968 \text{ kW}$$

$$= 114.04 \text{ kW}$$

- 48.** A circular water tank of 2 m diameter has a circular orifice of diameter 0.1 m at the bottom. Water enters the tank steadily at a flow rate of 20 litre/s and escapes through the orifice. The coefficient of discharge of the orifice is 0.8. Consider the acceleration due to gravity as 9.81 m/s<sup>2</sup> and neglect frictional losses. The height of the water level (in m, round off to two decimal places) in the tank at the steady state, is \_\_\_\_.

**Ans.** 0.52

**Sol.** Assuming, H is the level of water in the circular tank



Discharge through orifice = water enters in the tank

$$C_d \cdot a \sqrt{2gH} = 20 \times 10^{-3}$$

$$\Rightarrow 0.8 \times \frac{\pi}{4} (0.1)^2 \times \sqrt{2 \times 9.81 \times H}$$

$$= 20 \times 10^{-3}$$

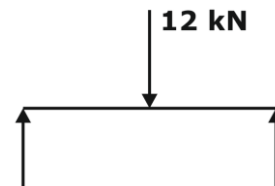
$$\Rightarrow H = 0.5164 \text{ m}$$

- 49.** A simply supported prismatic concrete beam of rectangular cross-section, having a span of 8 m. is prestressed with an effective prestressing force of 600 kN. The eccentricity of the prestressing tendon is zero at supports and

varies linearly to a value of e at the mid-span. In order to balance an external concentrated load of 12 kN applied at the mid-span, the required value of e (in mm. round off to the nearest integer) of the tendon, is \_\_\_\_.

**Ans.** 40 mm

**Sol.**



$$M = \frac{Wl}{4} = \frac{12 \times 8}{4} = 24 \text{ kN-m}$$

$$M = P \cdot e$$

$$24 \text{ kN-m} = 600 \text{ kN} \times e$$

$$\rightarrow e = 0.04 \text{ m}$$

$$\rightarrow e = 40 \text{ mm}$$

- 50.** Consider the system of equations

$$\begin{bmatrix} 1 & 3 & 2 \\ 2 & 2 & -3 \\ 4 & 4 & -6 \\ 2 & 5 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \\ 2 \\ 1 \end{bmatrix}$$

The value of  $x_3$  (round off to the nearest integer) is \_\_\_\_.

**Ans.** 3

**Sol.** Solving the above matrix by multiplication

$$x_1 + 3x_2 + 2x_3 = 1 \quad \dots(1)$$

$$2x_1 + 2x_2 - 3x_3 = 1 \quad \dots(2)$$

$$4x_1 + 4x_2 - 6x_3 = 2 \quad \dots(3)$$

$$2x_1 + 5x_2 + 2x_3 = 1 \quad \dots(4)$$

Solving equation (1) and (2) eliminating  $x_1$  we get,

$$\cancel{2x_1} + 6x_2 + 4x_3 = 2$$

$$\cancel{2x_1} + 2x_2 - 3x_3 = 1$$

$$\underline{\quad - \quad + \quad - \quad}$$

$$4x_2 + 7x_3 = 1 \quad \dots\dots(5)$$

Solving equation (3) and (4) eliminating  $x_1$ , we get

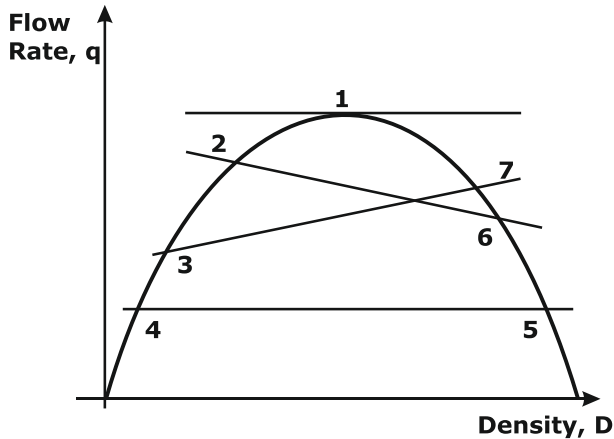
$$\begin{array}{r} 4x_1 + 4x_2 - 6x_3 = 2 \\ 4x_1 + 10x_2 + 4x_3 = 2 \\ \hline -6x_2 + 10x_3 = 0 \quad \dots\dots(6) \end{array}$$

Solving equation (5) and (6) we get

$$\begin{array}{r} 4x_2 + 7x_3 = 1 \\ -6x_2 - 10x_3 = 0 \\ 24x_2 + 42x_3 = 6 \\ \hline -24x_2 - 40x_3 = 0 \\ \hline 2x_3 = 6 \end{array}$$

$$x_3 = 3$$

51. The relationship between traffic flow rate ( $q$ ) and density ( $D$ ) is shown in the figure



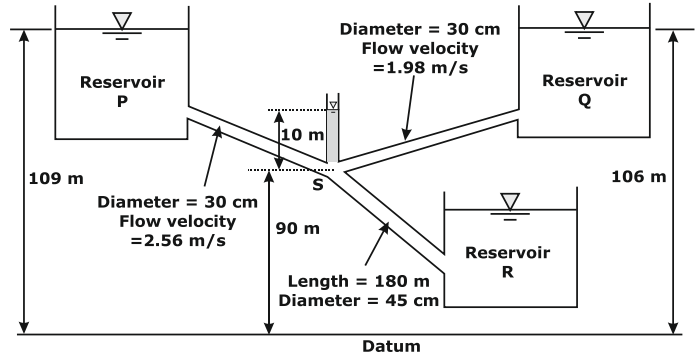
The shock wave condition is depicted by

- A. Flow with respect to point 1 ( $q_1 = q_{\max}$ )
- B. Flow changing from point 2 to point 6 ( $q_2 > q_6$ )
- C. Flow with respect to point 4 and point 5 ( $q_4 = q_5$ )
- D. Flow changing from point 3 to point 7 ( $q_3 < q_7$ )

Ans. B

52. Three reservoirs P, Q, and R are interconnected by pipes as shown in the figure (not drawn to the scale). Piezometric head at the junction S of

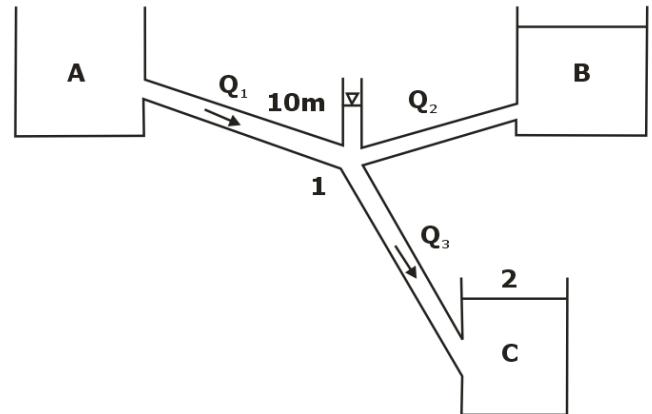
the pipes is 100m. Assume acceleration due to gravity as  $9.81 \text{ m/s}^2$  and density of water as  $1000 \text{ kg/m}^3$ . The length of the pipe from junction S to the inlet of reservoir R is 180 m.



Considering head loss only due to friction (with friction factor of 0.03 for all the pipes), the height of water level in the lowermost reservoir R (in m, round off to one decimal place) with respect to the datum, is \_\_\_\_\_.

Ans. 97.51

Sol.



We know that,  $Q_s = Q_{B1} + Q_{B2}$

By continuity equation,

$$\Rightarrow Q_s = A_1V_1 + A_2V_2$$

$$= Q = \frac{\pi}{4} \times 0.3^2 \times 2.56 + \frac{\pi}{4} \times 0.3^2 \times 1.98$$

$$= 0.3209 \text{ m}^3/\text{s}$$

Apply energy equation at 1 and 2

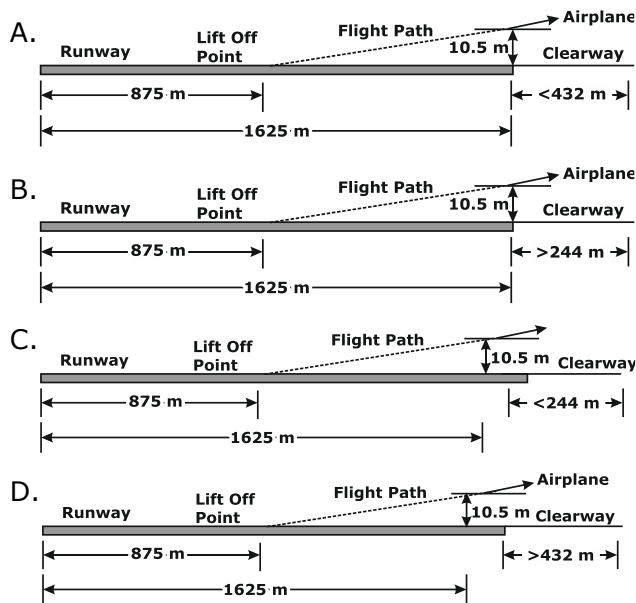
$$\therefore H_1 = H_2 + h_f$$

$$100 = z + \frac{8Q_3^2}{z^2g} \times \frac{fL_3}{D_3^5}$$

$$\Rightarrow 100 = z + \frac{8 \times 0.3209^2}{z^2g} \times \frac{0.03 \times 180}{0.45^5}$$

$$\Rightarrow z = 97.51 \text{ m}$$

53. The appropriate design length of a clearway is calculated on the basis of 'Normal Take-off condition. Which one of the following options correctly depicts the length of the clearway? (Note: None of the options are drawn to scale)



Ans. A

Sol. For standard case, of take-off, Clearway should not be more than

$$\frac{1}{2} \left( 1.5 \times \text{take off distance} - 1.15 \times \text{left off distance} \right)$$

Here, clearway

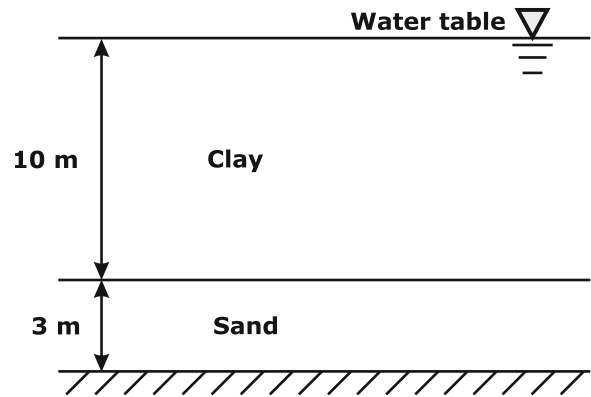
$$= \frac{1}{2} (1.15 \times 1625 - 1.15 \times 875)$$

$$= 431.25 \text{ m}$$

So, clearway is less than 432 m

54. A 10 m thick clay layer is resting over a 3 m thick sand layer and is submerged. A fill of 2 m thick sand with unit weight of 20 kN/m<sup>3</sup> is

placed above the clay layer to accelerate the rate of consolidation of the clay layer. Coefficient of consolidation of clay is  $9 \times 10^{-2}$  m<sup>2</sup>/year and coefficient of volume compressibility of clay is  $2.2 \times 10^{-4}$  m<sup>2</sup>/kN. Assume Taylor's relation between time factor and average degree of consolidation.



The settlement (in mm, round off to two decimal places) of the clay layer, 10 years after the construction of the fill, is

Ans. 18.8

Sol.

$$\Delta \bar{\sigma} = 40 \text{ kN/m}^2$$

$$\Delta H = m_v \times H_o \times \Delta \bar{\sigma}$$

$$= 2.2 \times 10^{-4} \times 10 \times 40$$

$$= 0.88 \text{ m}$$

$$= 88 \text{ mm} \rightarrow \text{Total consolidation}$$

$$T_v = \frac{c_v t}{d^2} = \frac{9 \times 10^{-2} \times 10}{5^2} = .036$$

$$T_v = \pi/4 u^2 V < 60\%$$

$$U = 21.4\%$$

$$\text{After layer settlement} = .214 \times 88 = 18.8 \text{ mm}$$

55. The length and bearings of a traverse PQRS are

Segment	Length(m)	Bearing
PQ	40	80°
QR	50	10°
RS	30	210°

The length of line segment SP (in m, round off to two decimal places), is

**Ans.** 44.802

**Sol.**

Segment	Length	Bearing	Lat.(lcosθ)	Dep.(lsinθ)
PQ	40	80	6.945	39.392
QR	50	10	49.250	8.682
RS	30	210	-25.980	-15
SP	l	θ	lcosθ	lsinθ

$$\Sigma L = l \cos \theta + 30.215 = 0$$

$$\Sigma D = l \sin \theta + 33.081 = 0$$

$$l \cos \theta = -30.215$$

$$l \sin \theta = -33.081$$

$$l = \sqrt{(30.215)^2 + (33.081)^2}$$

$$l = 44.802 \text{ m}$$

\*\*\*\*



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