

**QUESTION-1 — NAT**

Find the value of  $I$ . If  $C : |z| = 1$

$$I = \int_C iz dz$$

**SOLUTION: (1)**

$$= \int_0^{2\pi} (i\tilde{n}) e^{i\tilde{n}} d\tilde{n}$$

$$= \int_0^{2\pi} i^2 e^{2i\tilde{n}} d\tilde{n}$$

$$= -\frac{1}{2i} \frac{e^{2i\tilde{n}}}{2i}$$

$$C : |z| = 1 \Rightarrow z = e^{i\tilde{n}}$$

(unit circle)

$$dz = ie^{i\tilde{n}} d\tilde{n}$$

$$0 \leq \tilde{n} \leq 2\pi$$

$$= -\frac{1}{2i} \left[ \frac{e^{4i\tilde{n}}}{4i} - \frac{e^{0}}{4i} \right] = -\frac{1}{2i} \left[ \frac{1}{4i} - \frac{1}{4i} \right]$$

$$e^{2\pi i} = 1 \Rightarrow e^{4\pi i} = 1$$

**QUESTION-2 — MCQ**

$\frac{381}{274}$  will be equal to

(a) 323

(b)  $3^{40}$

(c) 369

(d)  $3^{46}$

**SOLUTION: (a)**

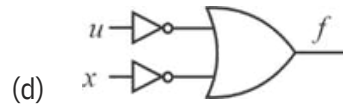
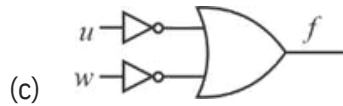
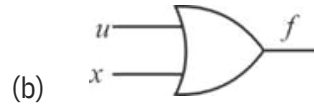
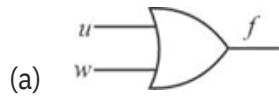
$$\frac{381}{274} = (381 \cdot 31)^{\frac{1}{3}}$$

$$(369)^{\frac{1}{3}}$$

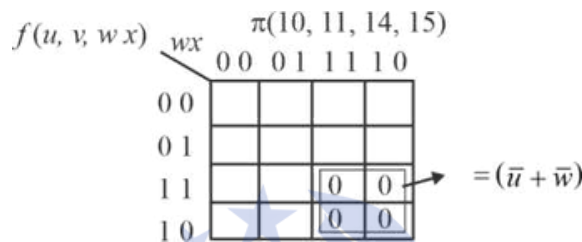
$$= 3^{23}$$

**QUESTION-3 — MCQ**

$$f = (u + v + w + x)(u + v + w + x)(u + v + w + x)(u + v + w + x)$$



**SOLUTION: (c)**



**QUESTION-4 — MCQ**

If a signal  $x(t) = -t^2 [u(t+4) - u(t-4)]$  given. Then the value of  $I$ .

$$I = \int_{-\infty}^{\infty} x(t) \cdot \delta(t+3) dt$$

(a) -9

(b) 9

(c) 1

(d) -1

**SOLUTION: (a)**

$$I = \int_{-\infty}^{\infty} x(t) \cdot \delta(t+3) dt$$

$$= -t^2; -4 \leq t \leq 4$$

$$= 0; \text{ otherwise}$$

$$I = \int_{-4}^4 -t^2 \cdot \delta(t+3) dt = -(-3)^2 = -9$$

**QUESTION-5 — NAT**

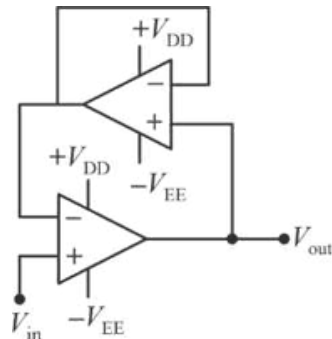
A continuous time periodic signal  $x(t) = 1 + 2\cos(2\delta t) + 2\cos(4\delta t) + 2\cos(6\delta t)$  is given, then the value of  $\frac{1}{T} \int_0^T |x(t)|^2 dt$  will be \_\_\_\_\_.

**SOLUTION: (7)**

$$\frac{1}{T} \int_0^T |x(t)|^2 dt = (1)^2 + 2 + 2 + 2 = 7$$

**QUESTION-6 — MCQ**

Assuming ideal op-amp, the circuit represent is a



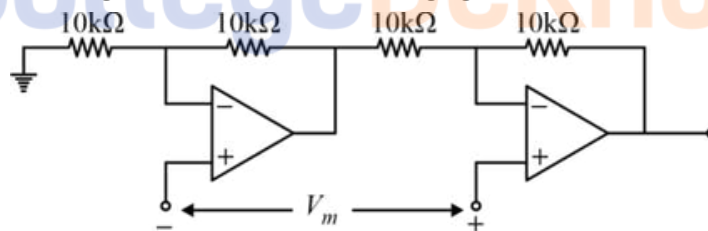
- (a) Logarithmic amplifier
- (b) Diff. amplifier
- (c) Summing amplifier
- (d) Buffer

**SOLUTION: (D)**

Buffer

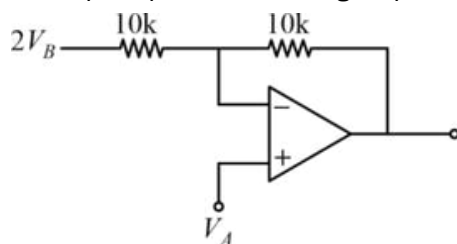
**QUESTION-7 — NAT**

The op-amp in the following circuit are ideal. The voltage gain of the circuit is \_\_\_\_\_.



**SOLUTION: (2)**

First op-amp is non inverting amplifier, so that output will be two times of the input.



$$((1+1)V_A - 2V_B)$$

$$V_0 = 2V_A - 2V_B$$

$$= 2(V_A - V_B) = 2V_{in}$$

**QUESTION-8 — NAT**

A low pass filter is given in frequency domain  $H(\omega) = \begin{cases} 1 & |\omega| \leq 200 \\ 0 & \text{else} \end{cases}$ . If  $h(t)$  is the time domain signal of the filter then the value of  $h(0)$  will be

**SOLUTION: (200)**

$$h(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} H(\omega) e^{j\omega t} d\omega$$

$$h(0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} H(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-200}^{200} 1 d\omega$$

$$h(0) = \frac{400}{2\pi} = 200$$

**QUESTION-9 — MCQ**

400 volt D.C series motor with zero series resistance, If load torque ( $T_L = 3 \text{ Nm}$ ). If initially motor draws 40A. Now, if motor speed is half of rated speed then the value of required series resistance [Use =  $I_a \omega$ ]

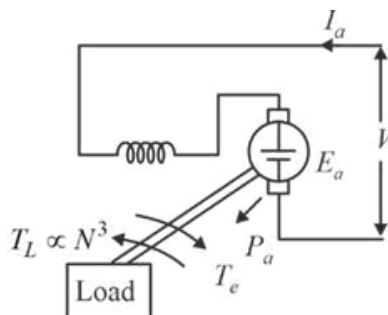
(a)  $4.67 \Omega$

(b)  $46.7 \Omega$

(c)  $22 \Omega$

(d)  $0 \Omega$

**SOLUTION: (c)**



$T_e = T_L$  (under S.S condition)

$$T_e = k' \omega I_a$$

$$\boxed{T_e \propto I_a^2}$$

$$T_L \propto N^3$$

$$I_a^2 \propto N^3$$

$$I_{a2} = \sqrt{\left(\frac{1}{2}\right)^3} \times 40 = 14.1421 \text{ A}$$

$$Ea = k\phi N = V - I_a(R_a + R_{se})$$

$$N = \frac{V - I_a(R_a + R_{se})}{k\phi}$$

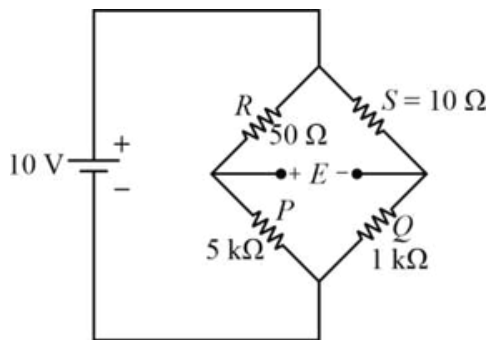
$$\frac{0.5N^1}{N^1} = \frac{400 - 14.142 \times R}{400 - 0} \times \frac{14.142}{14.142}$$

$$R_{ext} = 23.2 \Omega$$

#### QUESTION-10 — NAT

For the given wheat stone bridge, determine the sensitivity of the  $E$  if the value of  $R$  is changed in \_\_\_\_\_  $\text{mV}/\Omega$ .

**SOLUTION: (1.96)**



$$V_{Bri} = V^+ - V^-$$

$$= 10 \frac{1000}{1000 + 10} - \frac{5000}{5000 + 50}$$

$$V_{Bri} = 1.96 \text{ mV for } \Delta R = 1 \Omega$$

$$S_{Bri} = 1.96 \frac{\text{mV}}{\Omega}$$

**QUESTION-11 — NAT**

$y[n] = s[x[n]]$  is disc LTI system

$s[x[n]] = \begin{cases} x[n] + x[n-1] + x[n-2] & n \in \{0, 1, 2\} \\ x[n] & \text{otherwise} \end{cases}$ . For the input signal  $x[n]$ , the output  $y[n]$  is

**SOLUTION: (b)**

$$h[n] = \delta[n] + \delta[n-1] + \delta[n-2]$$

$$y[n] = x[n] * h[n]$$

$$y[n] = x[n] + x[n-1] + x[n-2]$$

**QUESTION-12 — MCQ**

$$V(t) = 300 \sin \omega t$$

$$I(t) = 10 \sin \left( \omega t + \frac{\pi}{6} \right) + 2 \sin \left( \omega t + \frac{\pi}{6} \right) + \sin \left( \omega t + \frac{\pi}{2} \right)$$

Input Power factor

- (a) 0.887 (b) 0.867  
(c) 0.847 (d) 1.0

**SOLUTION: (c)**

$$P(t) = V(t)I(t)$$

$$P_{\text{av}} = \frac{1}{2\pi} \int_0^{2\pi} P(t) d\omega t = \frac{300 \times 10 \cos \frac{\pi}{6}}{2} = 1500 \times \frac{\sqrt{3}}{2} = 750\sqrt{3} \text{ W}$$

$$V_{\text{rms}} = \frac{300}{\sqrt{2}}$$

$$I_{\text{rms}} = \sqrt{\frac{10^2}{2} + \frac{4^2}{2} + \frac{1^2}{2}} = \sqrt{\frac{105}{2}}$$

$$S = V_{\text{rms}} I_{\text{rms}} = \frac{300 \times \sqrt{105}}{2}$$

$$\cos \phi = \frac{P}{|S|} = \frac{750\sqrt{3}}{150\sqrt{105}} = \frac{5\sqrt{3}}{\sqrt{105}} = 0.847$$

**QUESTION-13 — MCQ**

Table 1st order LTI System

$T$	0.6	1.6	2.6	10	$\square$
Output	0.78	1.65	2.18	2.98	3

- (a) 1 (b) 2  
(c) 3 (d) 4

**SOLUTION: (b)**

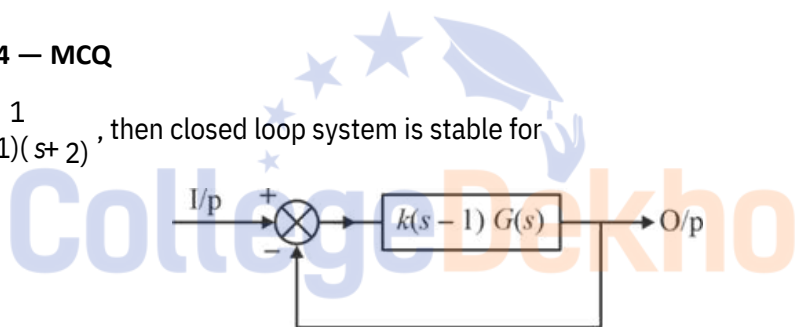
$$\text{Output} = V \square (1 - e^{-t/\square}) = 3(1 - e^{-t/\square})$$

$$0.78 = 3(1 - e^{-0.6/\square})$$

$$\square = 2$$

**QUESTION-14 — MCQ**

$G(s) = \frac{1}{(s+1)(s+2)}$ , then closed loop system is stable for



- (a) Stable for  $k > 2$  (b) Unstable for  $k > 2$   
(c) Stable for  $k > 1$  (d) Unstable for  $k < 1$

**SOLUTION: (b)**

$$G(s) = \frac{k(s-1)}{(s+1)(s+2)}$$

$$1 + G(s) = 1 + \frac{k(s-1)}{(s+1)(s+2)}$$

$$s^2 + 3s + 2 + ks - k = 0$$

$$s^2 + s[k+3] + (2-k) = 0$$

$$2 - k > 0$$

$$k < 2$$

Hence the system is unstable for  $k > 2$

**QUESTION-15 — MCQ**

$$A = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}, B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, C = \begin{bmatrix} 1 & 0 \end{bmatrix}$$

$$\dot{x}(t) = Ax(t) + Br(t), y(t) = cx(t)$$

Sum of magnitude of poles \_\_\_\_\_.

- (a) 2 (b) 3  
(c) 4 (d) 5

**SOLUTION: (b)**

$$A = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}, B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, C = (1, 0)$$

|Poles|

$$|sI - A| = 0$$
$$s^2 + 3s + 2 = 0$$

$$s = -1, -2$$

$$s_1 = -1$$

$$s_2 = -2$$

$$s_1 + s_2 = -3$$

$$|s_1 + s_2| = 3.$$

**QUESTION-16 — MCQ**

A 3-phase, 400 V, 4 pole, 50 Hz star connected induction motor has the following parameters referred to the stator:

$$R_s = 1 \Omega, X_s = X_r = 2 \Omega$$

Stator resistance, magnetizing reactance and core loss of the motor are neglected. The motor is running with constant V/f control from a drive. For maximum starting torque, the voltage and frequency output respectively from the drive is closest to,

- (a) 400 V and 50 Hz (b) 300 V and 37.5 Hz  
(c) 200 V and 25 Hz (d) 100 V and 12.5 Hz



**SOLUTION: (d)**

$$S_{T(\max)} = \frac{R_r}{(X_s + X_r)}$$

$$S_{T(\max)} = \frac{1}{4} S_{T(\max)} \propto \frac{1}{f}$$

$$\frac{S_{T(\max)_2}}{S_{T(\max)_1}} = \frac{f_1}{f_2} = \frac{50}{f_2}$$

$$f_2 = 50 \times \frac{1}{4} = 12.5 \text{ Hz}$$

$$\frac{V}{f} = \text{Constant} \propto f$$

$$V_2 = \frac{f_2}{f_1} V_1$$

$$= \frac{12.5}{50} \times 400 = 100 \text{ V}$$

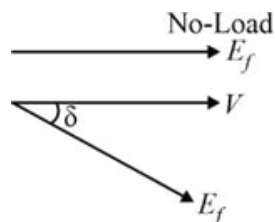
**QUESTION-17 — NAT**

The induced emf in a 3.3 kV, 4-pole, 3-phase star connected synchronous motor is considered to be equal and in phase with the terminal voltage under no load condition on application of a mechanical load, the induced emf phasor is deflected by angle  $2^\circ$  mechanical with respect to the terminal phasor voltage. If synchronous reactance is  $2\Omega$  and stator resistance is negligible, then the motor armature current magnitude in a ampere during load condition is \_\_\_\_\_.

**SOLUTION: (66.49)**

$$\delta = \frac{P}{2} S_{\text{mech}} = \frac{4}{2} \times 2 = 4^\circ$$

$$I_a X_s = \sqrt{E_f^2 + V^2 - 2VE_f \cos \delta}$$



$$E_{fph} = V_{ph} = \frac{3.3 \times 10^3}{\sqrt{3}}$$

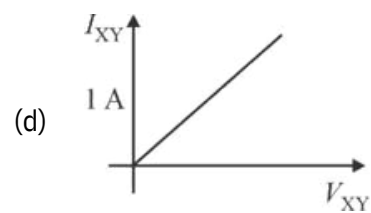
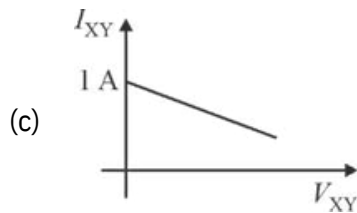
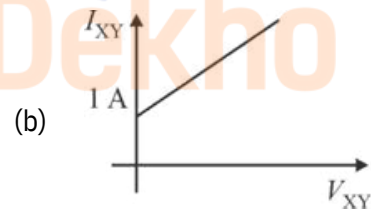
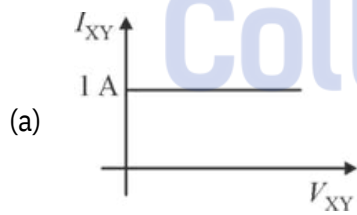
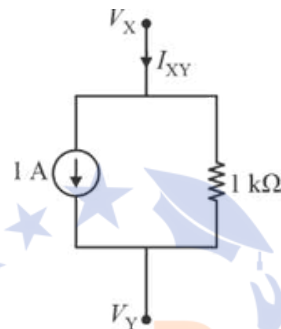
$$I_a X_s = V \hat{\delta} \sqrt{2 - 2 \cos \delta}$$

$$I_a = \frac{3.3 \times 10^3}{\sqrt{3} \hat{\delta} 2} \hat{\delta} \sqrt{2 - 2 \cos 40^\circ}$$

$$I_a = 66.49 \text{ A}$$

**QUESTION-18 — MCQ**

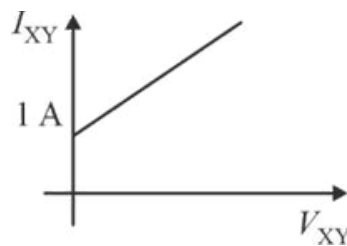
The I-V characteristics of the elements between the nodes X and Y is best depicted



**SOLUTION: (b)**

$$V_{XY} = (I_{XY} - 1) 1 \text{ k}\Omega$$

$$I_{XY} = 1 + \frac{V_{XY}}{1 \text{ k}\Omega}$$



**QUESTION-19 — NAT**

$$V = x^2 + x + y^2 + 1$$

Determine the value of rate of change of  $V$  at origin in the direction of  $(1, 2)$ .

(Round off to nearest integer)

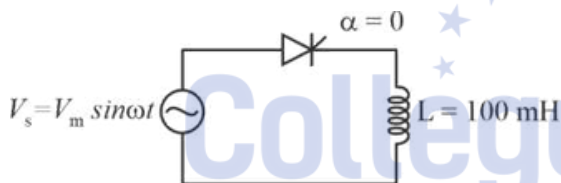
**SOLUTION: (0)**

$$\hat{A} = a_x \hat{x} + 2a_y \hat{y} \quad A = \frac{a_x \hat{x} + 2a_y \hat{y}}{\sqrt{5}}$$

$$\nabla V = (2x+1)a_x \hat{x} + 2ya_y \hat{y}$$

$$D \nabla V = \nabla V \cdot \hat{A} = \frac{(2x+1) + 4y}{\sqrt{5}} \Big|_{\substack{x=0 \\ y=0}} = \frac{1}{\sqrt{5}} = 0.45 \sim 0$$

**QUESTION-20 — NAT**



The value of peak inductor current will be \_\_\_\_

**SOLUTION: (c)**

$$V_m \sin \omega t = L \frac{di}{dt}$$

$$di = \frac{V_m \sin \omega t}{L} dt$$

$$\int di = \frac{V_m}{L} \int \sin \omega t dt$$

$$i = \frac{V_m}{\omega L} (-\cos \omega t) + k$$

Where  $\omega t = 0$

$$i = 0$$

$$0 = \frac{V_m}{\omega L} (-1) + k$$

$$k = \frac{V_m}{\omega L}$$

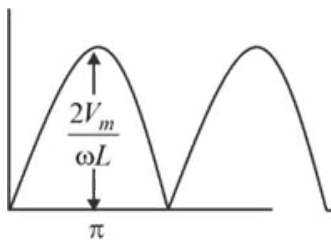
$$i = \frac{V_m}{\omega L} (1 - \cos \omega t)$$

Maxm current will occur when  $\omega t = \delta$

$$(i)_{mx} = \frac{2V_m}{\omega L}$$

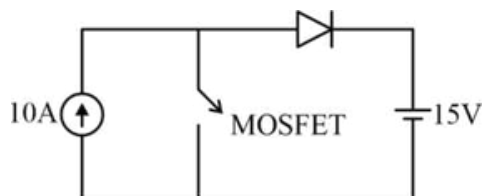
$$= \frac{2 \hat{230} \hat{\sqrt{2}}}{2 \hat{50} \hat{100} \hat{10}}$$

$$= 20.707 \text{ Amp.}$$



### QUESTION-21 – NAT

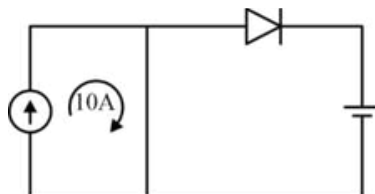
In the circuit with ideal devices power MOSFET is turn ON for  $D = 0.4$ . If input current is constant then the power delivered by the current source.



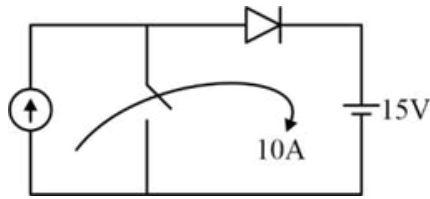
### SOLUTION: (90)

Mode-1

SW  $\rightarrow$  ON

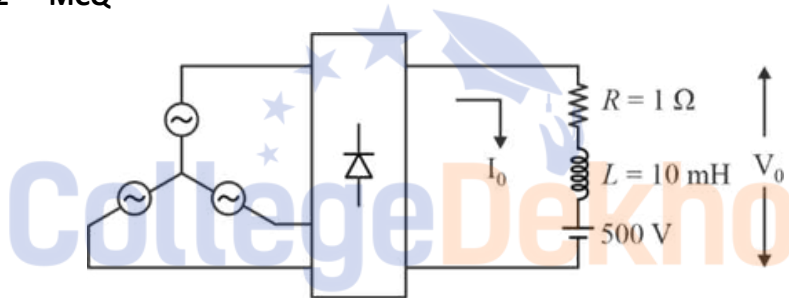


Power loss = 0



$$\begin{aligned}
 &\text{Energy loss } 10 \times 15 \times T_{OFF} \\
 &= 150 (1 - \square) T \\
 &\text{Average power loss} = \frac{0 + 150(1 - \square) T}{T} \\
 &= 150 (1 - 0.4) \\
 &= 150 \times 0.6 \\
 &= 90 \text{ W}
 \end{aligned}$$

**QUESTION-22 — MCQ**



$$V = 400 \frac{\sin \omega t}{\omega} + \frac{\cos \omega t}{3 \omega}$$

Power loss in resistor = 64W. The value of firing angle is

- (a) 0°
- (b) 35.9°
- (c) 40.5°
- (d)

**SOLUTION: (b)**

$$\text{Power loss} = I_0^2 R$$

$$64 = 2 I_0^2 (1)$$

$$I_0 = \sqrt{\frac{64}{2}} = 8 \text{ Amp}$$

$$I_0 = \frac{V_0 - E}{R}$$

$$8 = \frac{400 \frac{\sin \omega t}{\omega} + \frac{\cos \omega t}{3 \omega} - 500}{1}$$

$$8 = 400 \frac{\sin \omega t}{\omega} + \frac{\cos \omega t}{3 \omega} - 500$$

$$508 = 400 \frac{\ddot{\theta}}{\theta} + \frac{\cos \theta \ddot{\theta}}{3 \ddot{\theta}}$$

$$1.27 = 1 + \frac{\cos \theta}{3}$$

$$\frac{\cos \theta}{3} = 0.27$$

$$\cos \theta = 0.81$$

$$\theta = 35.9^\circ$$

### QUESTION-23 — MCQ

$V_1$  and  $V_2$  are Eigen vectors of real symmetric matrix of  $3 \times 3$  corresponding to distinct Eigen values then

- (a)  $V_1^T V_2 = 0$  (b)  $V_1 - V_2 = 0$   
 (c)  $V_1^T V_2 \neq 0$  (d)  $V_1 + V_2 = 0$

### SOLUTION: (a)

We know that Eigen vectors of real symmetric matrix for different Eigen values are orthogonal i.e.  $V_1 - V_2 = 0$  and we know that dot product is  $V_1^T V_2 = V_1^T V_2$ , so  $V_1^T V_2 = 0$ .

### QUESTION-24 — MCQ

$$A = \begin{bmatrix} 1 & 1 & 1 \\ -1 & -1 & -1 \\ 0 & 1 & 1 \end{bmatrix} \quad B = \begin{bmatrix} 1/3 \\ -1/3 \\ 0 \end{bmatrix}, \text{ then } AX = B \text{ has}$$

- (a) No solution (b) Infinite solutions  
 (c) Unique solution (d) Two solutions

### SOLUTION: (b)

$$[A:B] = \begin{bmatrix} 1 & 1 & 1 & : & 1/3 \\ -1 & -1 & -1 & : & -1/3 \\ 0 & 1 & 1 & : & 0 \end{bmatrix} \xrightarrow{R_2 + R_1} \begin{bmatrix} 1 & 1 & 1 & : & 1/3 \\ 0 & 1 & 1 & : & 0 \\ 0 & -1 & -1 & : & -1/3 \end{bmatrix}$$

$$\xrightarrow{R_3 + R_2} \begin{bmatrix} 1 & 1 & 1 & : & 1/3 \\ 0 & 1 & 1 & : & 0 \\ 0 & 0 & 0 & : & 0 \end{bmatrix}$$

$$\rho(A) = 2 \text{ and } \rho(A : B) = 2$$

i.e.,  $\rho(A) = \rho(A : B) < \text{Number of variables}$ . It means infinite solutions exist.

**QUESTION-25 — MCQ**

If  $S : (x, y) \in \mathbb{R}^2$  and  $Z = x^2 + x + y^2 + 1$  then set of points  $S$  for which  $Z$  will be minimum is

- (a)  $S$  is finite
- (b)  $S$  contains only one point
- (c)  $S$  is empty
- (d)  $S$  is finite but it has more than one point

**SOLUTION: (b)**

$$Z_x = 2x + 1, Z_{xx} = 2, Z_y = 2y, Z_{yy} = 2, Z_{xy} = 0.$$

For critical points:  $Z_x = 0$  and  $Z_y = 0 \Rightarrow x = -\frac{1}{2}, y = 0$  will be critical point.

Now,  $rt - s^2 = (2)(2) - (0)^2 = 4 - 0 = 4 > 0$  and  $r = 2 > 0$ .

So, point will be point of minima.

Hence, set  $S$  contains only one point.

**QUESTION-26 — NAT**

Evaluate:  $\int_C izdz$  where  $C : |z| = 1$

**SOLUTION: (0)**

$$C: |z| = 1 \Rightarrow z = e^{i\theta}, dz = ie^{i\theta} d\theta, 0 \leq \theta < 2\pi$$

$$I = \int_C izdz = i \int_0^{2\pi} e^{i\theta} (ie^{i\theta}) d\theta = i^2 \int_0^{2\pi} (e^{2i\theta}) d\theta$$

$$= -\frac{1}{2i} \left[ \frac{e^{2i\theta}}{2i} \right]_0^{2\pi} = -\frac{1}{2i} \left[ \frac{e^{4\pi i} - 1}{2i} \right] = \frac{1}{4} [1 - 1] = 0$$

**QUESTION-27 — MCQ**

If  $P = \begin{pmatrix} 2 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix}$  then  $P^2$  will be

- (a)  $P$
- (b)  $P + I$
- (c)  $I$
- (d)  $2P - I$

**SOLUTION: (d)**

$$P^2 = P \cdot P = \begin{pmatrix} 2 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 2 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 4 & 2 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 2 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \cdot 2 - \begin{pmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad \dots(1)$$

Taking option (d)

$$2P - I = \begin{bmatrix} 2 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 2 \\ 1 \\ 0 \end{bmatrix} \quad \dots(2)$$

By (1) and (2)

$$P_2 = 2P - I$$

i.e. (d) is correct.

**QUESTION-28 — NAT**

Rate of change of  $V = x^2 + x + y^2 + 1$  at origin in the direction of point (1, 2) is \_\_\_\_\_ ?

**SOLUTION: (0.447)**

$$\text{Grad } V = \hat{i} \frac{\partial V}{\partial x} + \hat{j} \frac{\partial V}{\partial y} + \hat{k} \frac{\partial V}{\partial z}$$

$$= (2x + 1)\hat{i} + 2y\hat{j} + 0\hat{k}$$

$$(\text{Grad } V)P(0, 0) = \hat{i} + 0\hat{j} + 0\hat{k}$$

Now,  $P(0, 0)$  and  $Q(1, 2)$

$$\text{So, } \vec{PQ} = \hat{i} + 2\hat{j} \text{ and } |\vec{PQ}| = \sqrt{5}$$

$$\text{Required rate of change} = \frac{(\hat{i} + 2\hat{j}) \cdot (\hat{i} + 0\hat{j} + 0\hat{k})}{\sqrt{5}} = \frac{1}{\sqrt{5}} = 0.447$$

**QUESTION-29 — NAT**

In the distribution feeder, the value of  $\frac{R}{X} = 5$ . Then the value of power factor if maximum voltage drop in the feeder. (Upto three decimal places)

**SOLUTION: (0.981)**

Maximum voltage drop in the feeder leads to maximum voltage regulation.

$$\text{The power factor angle in the case of maximum voltage regulation is } \bar{\alpha} = \tan^{-1} \frac{X}{R}$$

$$\text{So, power factor} = \cos \bar{\alpha} = \cos \tan^{-1} \frac{X}{R} = \frac{R}{\sqrt{R^2 + X^2}} = \frac{1}{\sqrt{1 + 5^2}} = 0.981$$



**QUESTION-30 — NAT**

The Z-bus matrix is given, if a symmetrical fault (LLL) occurred at bus-2. Then the voltage at bus-1 after fault. Assume pre-fault no-load.

$$Z_{bus} = \begin{bmatrix} j0.059 & j0.061 & j0.038 \\ j0.061 & j0.093 & j0.066 \\ j0.038 & j0.066 & j0.116 \end{bmatrix} \quad Z_f = j0.007 \text{ p.u.}$$

**SOLUTION: (0.39)**

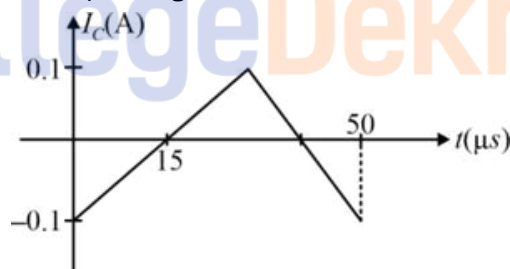
$$Z_{f(2)} = \frac{E}{Z_{E2} + Z_f} = \frac{E}{Z_{22} + Z_f} = \frac{0.038}{j0.093 + j0.007} = \frac{0.116}{j0.10} = -j1.16 \text{ p.u.}$$

$$V_1 = E - Z_{12} I_{f(2)}$$

$$= 1 - (j0.061)(-j1.16) = 1 - (0.7076) = 0.2924 \text{ p.u.}$$

**QUESTION-31 — NAT**

Supply voltage is 30 V. The capacitor current wave form of a buck converter is given below. Then the value of inductor if convert is operating in CCM.



**SOLUTION: (1.8)**

$$V_s = 30 \text{ V}$$

$$\Delta I_C = \Delta I_L = 0.1 \text{ A}$$

$$D = \frac{15 + 15}{50} = 0.6$$

$$\Delta I_L = \frac{D(1-D)V_s}{fL}$$

$$f = \frac{1}{50 \times 10^{-6}} = 20 \text{ kHz}$$

$$0.1 = \frac{0.6 \times 0.4 \times 30}{20 \times 10^3 \times L}$$

$$L = 1.8 \text{ mH}$$

**QUESTION-32 — NAT**

$$\begin{aligned} \dot{x}_1(t) &= 2x_2(t) \\ \dot{x}_2(t) &= u(t) \\ x_1(0) &= 1, x_2(0) = 0 \\ x_1(t) / t=1 &=? \end{aligned}$$

**SOLUTION: (2)**

$$A = \begin{pmatrix} 0 & 2 \\ 0 & 0 \end{pmatrix}, B = \begin{pmatrix} 0 \\ 1 \end{pmatrix}, x(0) = \begin{pmatrix} 1 \\ 0 \end{pmatrix}$$

$$X(s) = (sI - A)^{-1} (0x + (sI - A)^{-1} B \psi)$$

$$(sI - A)^{-1} = \begin{pmatrix} s & 0 \\ 0 & s \end{pmatrix}^{-1} = \begin{pmatrix} 1/s & 0 \\ 0 & 1/s \end{pmatrix}$$

$$(sI - A)^{-1} = \begin{pmatrix} 1/s & -2/s^2 \\ 0 & 1/s \end{pmatrix}$$

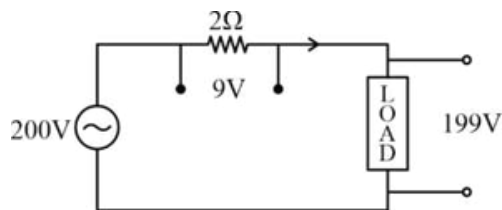
$$(sI - A)^{-1} B = \begin{pmatrix} 1/s & -2/s^2 \\ 0 & 1/s \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} -2/s^2 \\ 1/s \end{pmatrix}$$

$$X(s) = \begin{pmatrix} -2/s^2 \\ 1/s \end{pmatrix} \psi = \begin{pmatrix} -2/s^2 \\ 1/s \end{pmatrix} \frac{1}{s} = \begin{pmatrix} -2/s^3 \\ 1/s^2 \end{pmatrix}$$

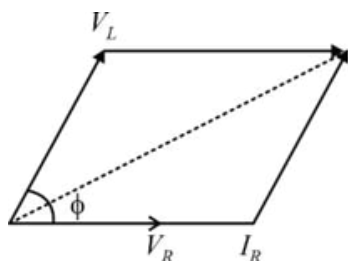
$$x_1(t) = 2$$

**QUESTION-33 — NAT**

For the circuit shown below, if load is inductive then the value of power absorbed by the load.



**SOLUTION: (79.5)**



$$PL = ?$$

$$I = \frac{9}{2} = 4.5A$$

$$V_s = V_R^2 + V_L^2 + 2VR \cdot V_L \cdot \cos \phi$$

$$2002 = 9^2 + 1992 + 2 \cdot 9 \cdot 139 \hat{\phi} \cos \phi$$

$$\cos \phi = 0.08878$$

$$P = V_L I \cos \phi = 79.5W$$

**QUESTION-34 — MSQ**

To synchronize an alternator to the grid, which instruments is/are required?

- (a) Voltmeter
- (b) Wattmeter
- (c) Stroboscope
- (d) Synchroscope

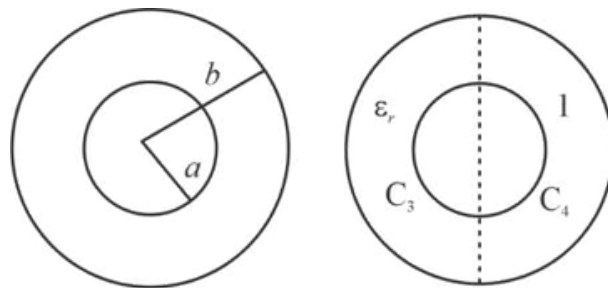
**SOLUTION: (a, d)**

Among the given options, voltmeter and Synchroscope are required.

**QUESTION-35 — NAT**

Find the relative permittivity for the given cylindrical capacitor.

Given  $C_2 = 5C_1$ ?



**SOLUTION: (9)**

$$C_1 = \frac{2\pi\epsilon_0 L}{\ln(b/a)}, C_3 = \frac{\pi\epsilon_0 L}{\ln(b/a)}, C_4 = \frac{\pi\epsilon_0 L}{\ln(b/a)}$$

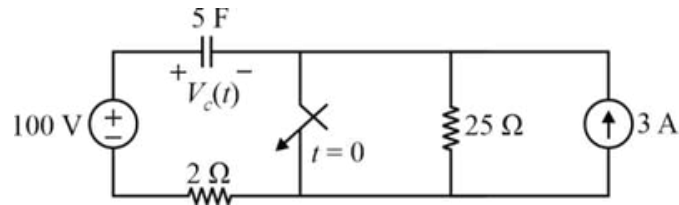
$$C_2 = C_3 + C_4$$

$$\pi \frac{\epsilon_0(\epsilon_r + 1)L}{\ln(b/a)} = \frac{5(2\pi\epsilon_0 L)}{\ln(b/a)}$$

$$\epsilon_r + 1 = 10 \Rightarrow \epsilon_r = 9$$

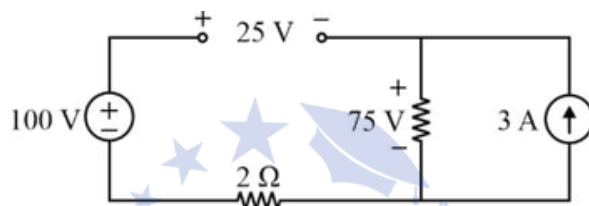
**QUESTION-36 — NAT**

For given below circuit the switch is will be closed at  $t = 0$  find the time ( $t$ ) at which  $V_c(t) = 50$  V.

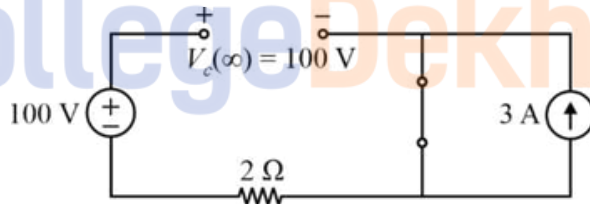


**SOLUTION: (?)**

At  $t < 0$  the circuit is :



At  $t = \infty$  :



$R_{eq}$  and  $C_{eq}$  can be calculated as :

$$R_{eq} = 2 \Omega$$

$$C_{eq} = 5$$

$$V_c(t) = 100 + [-5] \cdot \frac{75}{10} e^{-t/10}$$

$$50 = 100 - 75 \frac{t}{10}$$

$$75 \frac{t}{10} = 50$$

$$\frac{-t}{10} = \frac{\ln 50}{\ln 75}$$

$$t = 4.05 \text{ sec.}$$

**QUESTION-37 — MCQ**

Find the correct statement for amplifier

- (a) CS and CG both  $NI$  amp
- (b) CS I CG  $NI$
- (c) CS  $NI$  CG I
- (d) CS and CG both I.

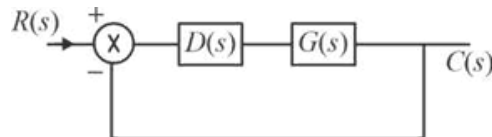
**SOLUTION: (b)**

Common Source → Inverting amplifier

Common Gate → Non Inverting amplifier

**QUESTION-38 — NAT**

If the phase margin of the given system is  $45^\circ$  at gain cross over frequency = 10, then the value of  $KD$ .



**SOLUTION: (0.1)**

$$D(s) = k + Ds$$

$$PM = 45^\circ$$

$$\omega_{gc} = 10 \text{ rad/sec}$$

$$PM = 180^\circ + \phi(\omega_{gc})$$

$$45^\circ = 180^\circ + \phi(\omega_{gc})$$

$$\phi(\omega_{gc}) = -135^\circ$$

$$G(s) = \frac{1000\sqrt{D}}{s(s+10)^2}$$

$$\phi(\omega) = \tan^{-1} kD\omega - 90^\circ - 2 \tan^{-1} \frac{\omega}{10}$$

$$\phi(\omega_{gc}) = \tan^{-1} 10kD - 90^\circ - 2 \tan^{-1} \frac{10}{10}$$

$$\phi(\omega_{gc}) = \tan^{-1} kD \hat{\omega} 10 - 90 - 90$$

$$\phi(\omega_{gc}) = \tan^{-1} kD \hat{\omega} 10 - 180^\circ$$

$$-135^\circ = \tan^{-1} kD \hat{\omega} 10 - 180^\circ$$

$$\tan^{-1} kD \hat{\omega} 10 = 45^\circ$$

$$\boxed{K_D = 0.1}$$

**QUESTION-39 — MCQ**

Good : Evil :: Genuine : \_\_\_\_\_.

- (a) Counter fold (b) Counter part  
(c) Counterfeit

**SOLUTION: (c)**

As Good is antonym of Evil

Thus, Genuine is antonym of Counterfeit.

**QUESTION-40 — MCQ**

Ramya \_\_\_\_\_ go to office yesterday because she \_\_\_\_\_ well.

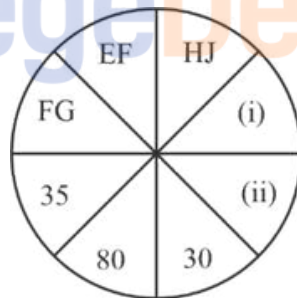
- (a) Couldn't, Wasn't (b)  
(c) (d)

**SOLUTION: (a)**

Couldn't, Wasn't

**QUESTION-41 — MCQ**

In the given figure, EF and HJ is coded as 30 and 80 respectively, then find (i) and (ii).



- (a)  
(b)  
(c)  
(d) EG/GE

**SOLUTION: (d)**

Here the product of alphabet position is the code, like  $E \times F = 5 \times 6 = 30$  and  $H \times J = 8 \times 10 = 80$

Thus,  $F \times G = 6 \times 7 = 42 \rightarrow$  (ii)

and  $35 = 5 \times 7 = E \times G$  or  $G \times E \rightarrow$  (i)

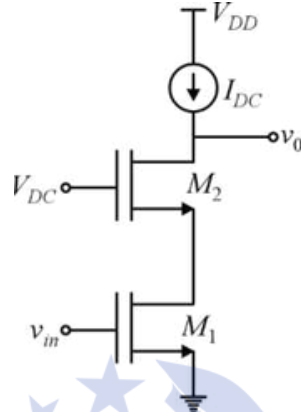
(i) and (ii) is EG/GE and HZ

**QUESTION-42 — MCQ**

For both M1 and M2 shown in the below circuit :

$$r_{o1} = r_{o2} = R_{ds}, \quad g_{m1} = g_{m2} = g_m$$

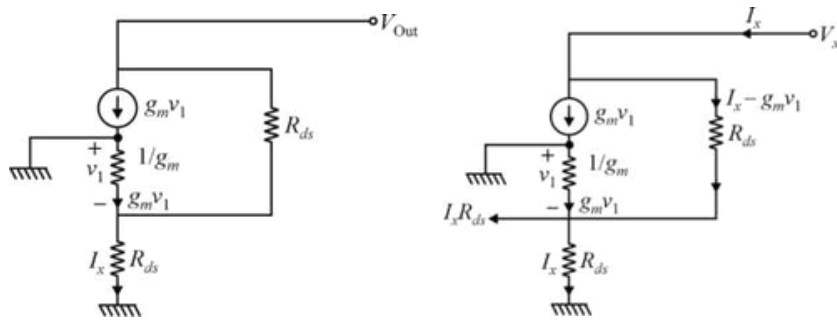
The output impedance of the circuit is \_\_\_\_\_.



- (a)  $(2R_{ds} + gmR_{ds})$  (b)  $(2R^2 + gmR_{ds})$   
 (c)  $(4R + gmR_{ds}^2)$  (d)  $(2R_{ds} + 2gmR_{ds})$

**SOLUTION: (a)**

The AC model of the circuit given in the question is shown below:



- (1)  $v_1 = 0 - I_x R_{ds}$   
 $v_1 = -I_x R_{ds}$   
 (2)  $V_x = (I_x - gm v_1) R_{ds} + I_x R_{ds}$   
 $V_x = (I_x + I_x R_{ds} gm) R_{ds} + I_x R_{ds}$   
 $V_x / I_x = ((1 + gm R_{ds}) R_{ds} + R_{ds})$

On calculating above equation we'll get:

$$\frac{V_x}{I_x} = (2R_{ds} + gmR_{ds}).$$

□□□